

Modernization of water turbine flow passages

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- **Virtual hydraulic laboratory**, developed as a result of numerous practical applications.
- **Computational Fluid Dynamics (CFD)** - established its strong presence in the hydropower industry as trusted engineering tool.
- Study and analysis of the hydraulic diagnostics allow developing an **upgrade strategy**
- Selected practical applications of **Computational Fluid Dynamics (CFD)** based on commercial software package (CFX).
- Selected practical applications of **Finite Element Analysis (FEA)** based on commercial software package (SolidWorks).



Reasons for modernization of water turbines

Reason 1 – Design deficiency – mechanical (structural)

- Frequent mechanical failures requiring extensive periodic repair work

Reason 2 – Change in operating parameters

- Changes in demand from the grid

Reason 3 – Change in hydraulic conditions

- Changing hydrological conditions, which occurred after many years of operation,

Reason 4 - Design deficiency possibly due to mistaken determination of hydrological conditions

- Most often in low-head installations

results of mechanical and hydraulic diagnostics along with preliminary developed solution require positive economic assessment for the decision to upgrade

Design upgrades methodology

Phase 1:

Hydraulic diagnostics of a fully homologous numerical model of the entire hydraulic system

- verification of CFD results with available field test results
- tuning the numerical model.

Phase 2:

Design optimization using general Evolutionary Algorithm (EA)

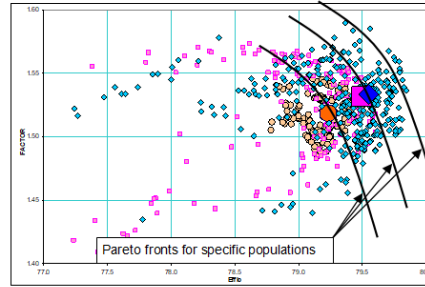
MODOA (Multi-Objective Design Optimization Algorithm)

EVOLUTIONARY STAGE

Series of CFD analyses for shapes: $S_1, S_2, \dots, S_{i-1}, S_i, \dots, S_n$

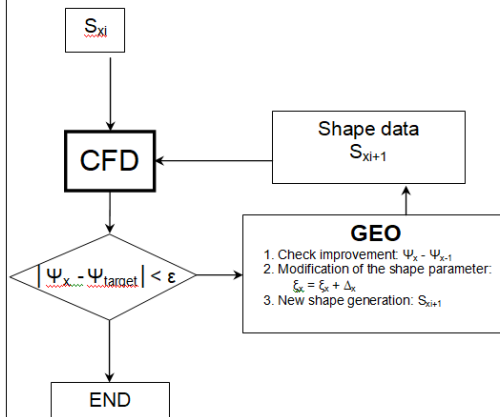
Calculation on set of shape parameters, which would bring best performances for the given population

Generation of next population: $S_{i+1}, \dots, S_{i+k}$

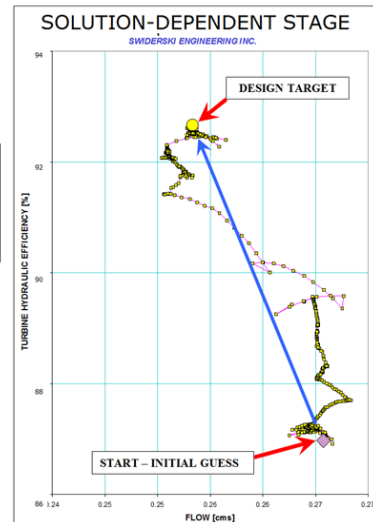


EVOLUTIONARY STAGE

SOLUTION-DEPENDENT STAGE

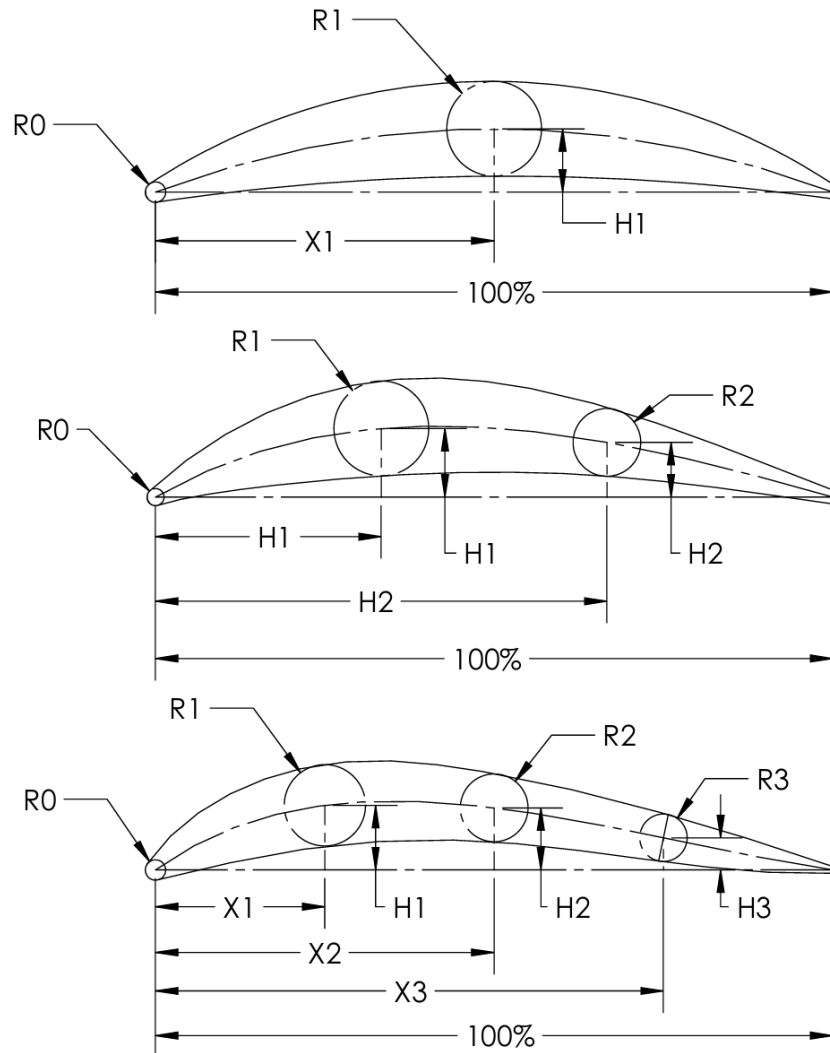


Ψ_x - quality factor
 ξ_x - active geometry parameter
 Δ_x - rate of change of ξ_x
 ϵ - proximity of the solution ($\epsilon \sim \Psi_{\text{target}}/1000$)



SOLUTION-DEPENDENT STAGE

MODOA (Multi-Objective Design Optimization Algorithm)



Shape manipulation is the result of manipulating the airfoil angle and the shape parameters, which determine the two-dimensional airfoil shape described by the parameters X_i , H_i , and R_i .

Usually the first two parameterization steps facilitate achieving relatively quickly a reasonable solution, although parameterization with steps with $n > 3$ are necessary to get final 2% to 4% gain in hydraulic efficiency

X_i , H_i , R_i , $i = 0 \dots n$

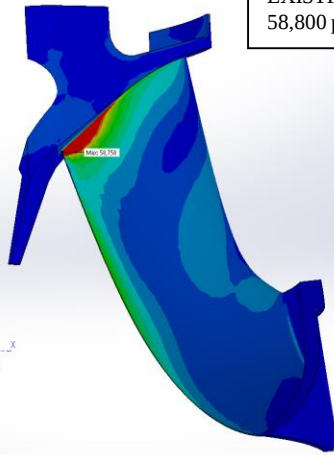
Stage 1: $n = 1$

Stage 2: $n = 2$

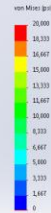
Stage 3: $n = 3$

EXAMPLE 1 - Design deficiency

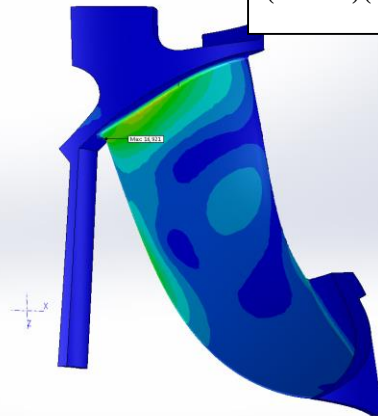
Model name: Isg_20Nov_ORIGDRA_Fp2
Study name: Static 110rps05
Post type: 200:node stress: Stress1



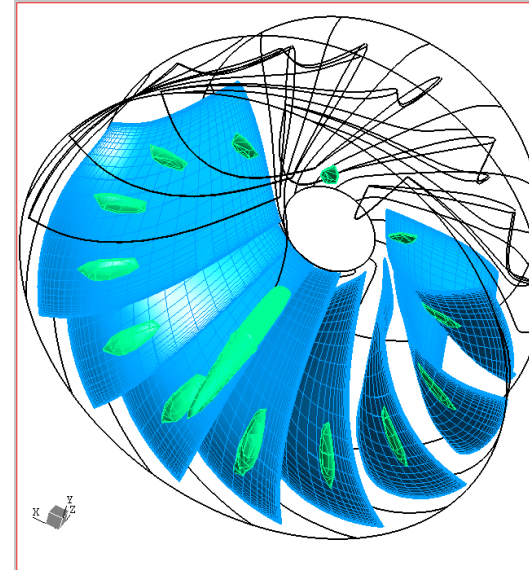
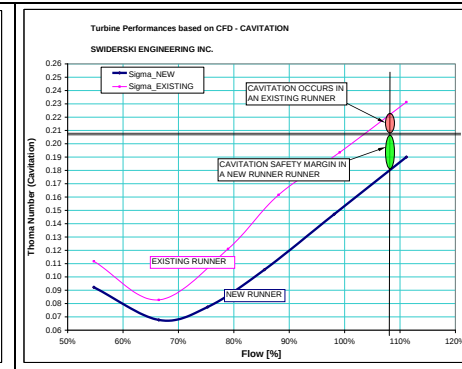
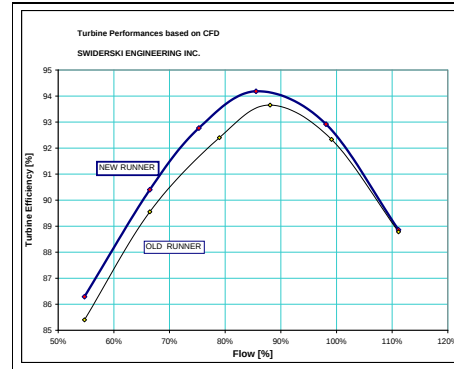
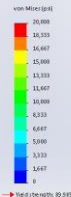
EXISTING BLADE, Max. combined stress
58,800 psi (405 MPa) (approx 70% of the Y.P.)



Model name: Isg_20Nov_2
Study name: Static 110rps05
Post type: 200:node stress: Stress1

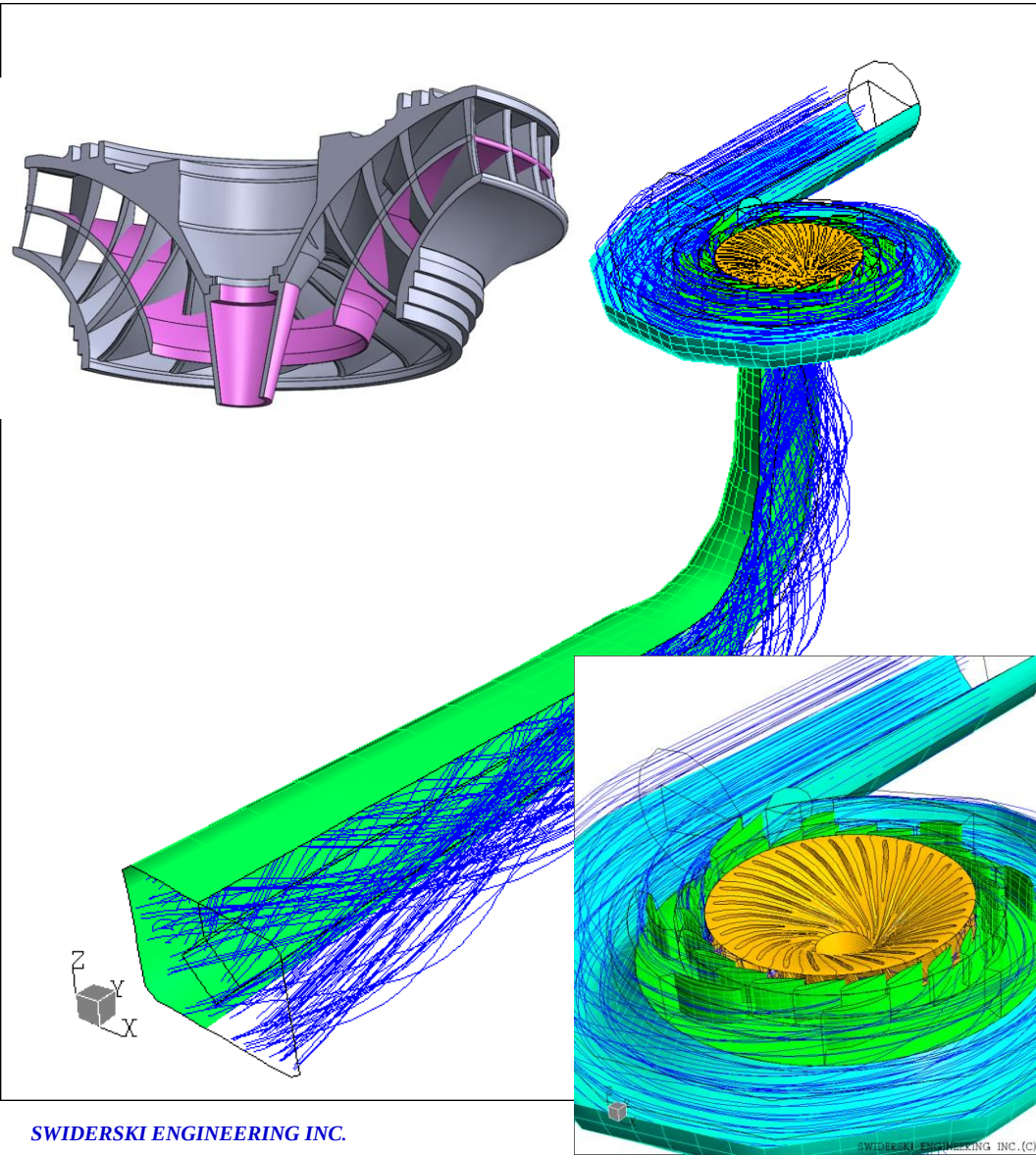


NEW BLADE, Max. combined stress 16,900 psi
(117 MPa) (approx 20% of the Y.P.)

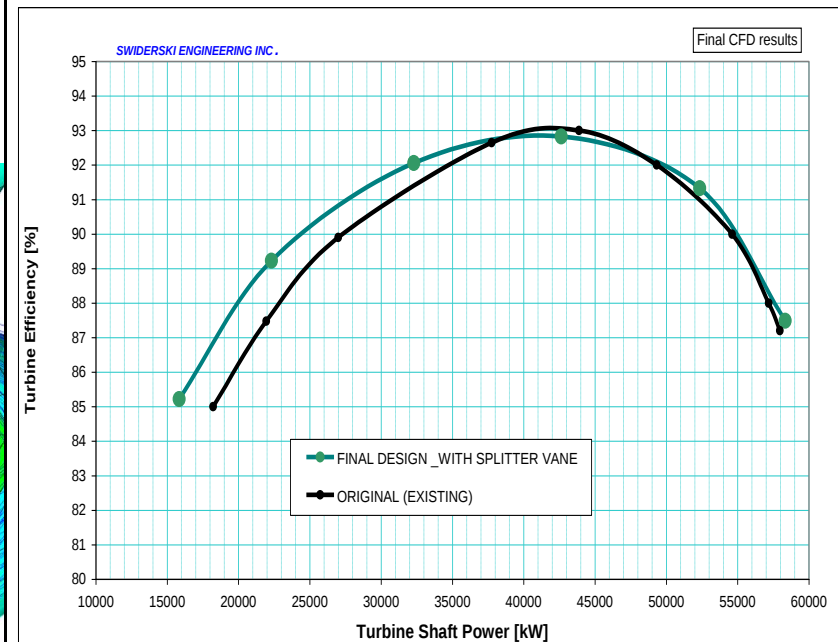


The goal: to reduce the frequency of repairs or eliminate them altogether. The rotor of the newly installed Francis turbine required a major overhaul every two years since its inception. Blade cracks and cavitation pitting required turbine disassembly and resulted in two months of downtime.

EXAMPLE 2 – Change in operating parameters

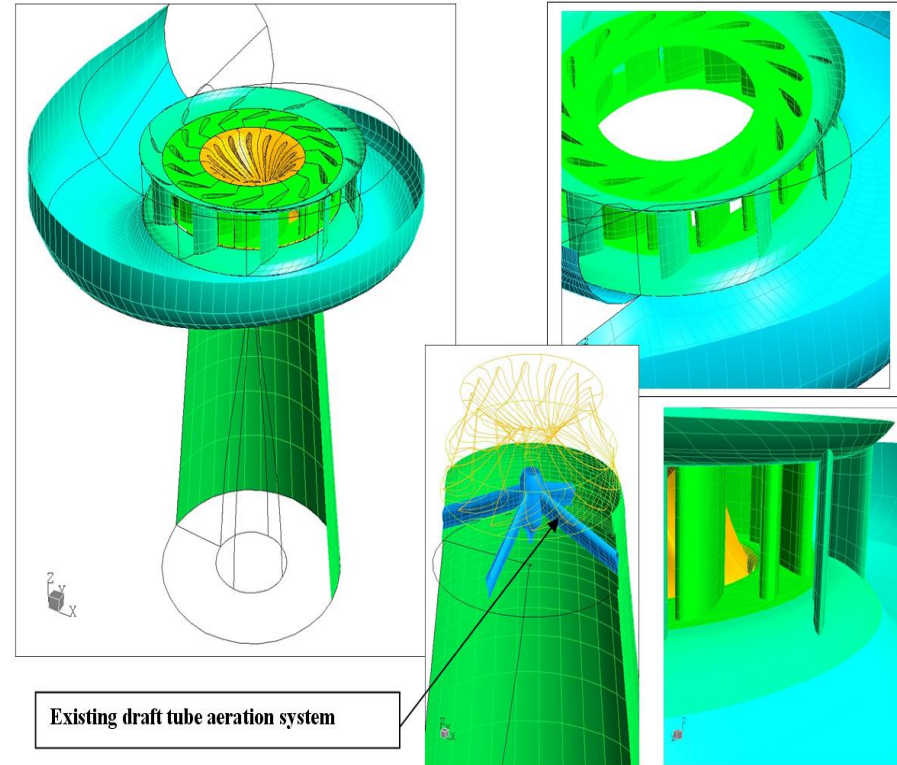
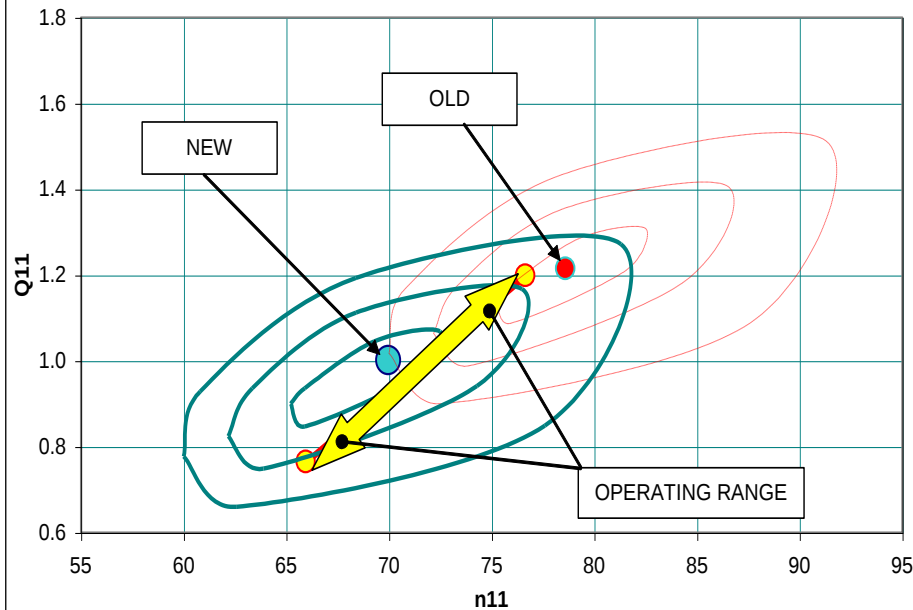


The original runner allowed for stable operation in the 75%-105% minimum load range. Changing hydrological conditions, which occurred after many years of operation, as well as demand imposed by the national electrical grid required additional operation of the turbine at 30%-60% load. However, within this range, operational instability in both the turbine set (increased vibrations) and the supply pipeline significantly exceeded acceptable standards.



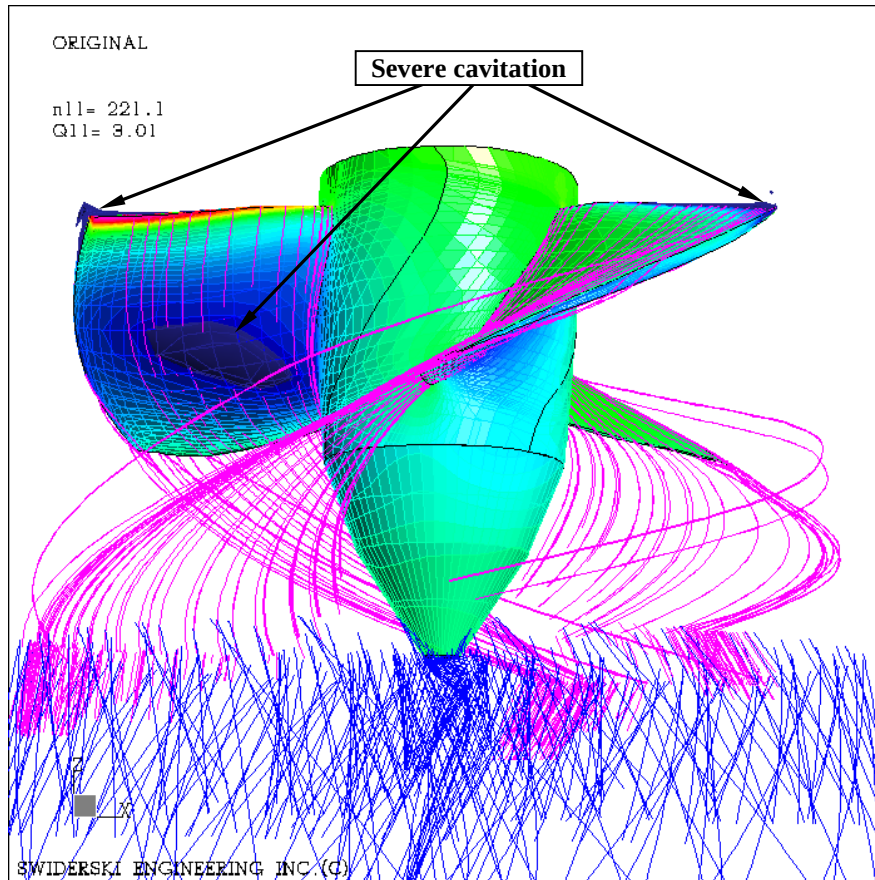
EXAMPLE 3 – Change in hydraulic conditions

Lushui Project
Hill chart position - NEW and OLD runners
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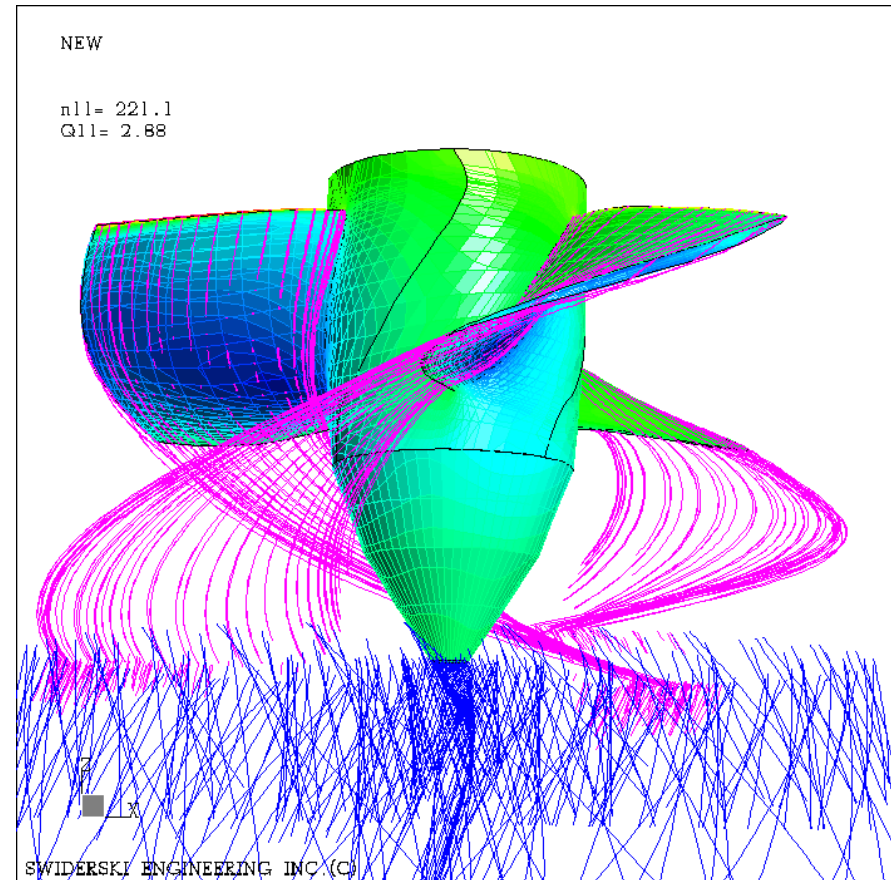


The configuration of the Lushui generating station and its complex hydrological conditions result in large head and flow variations at the dam, which affect the operation of the power-generating equipment. Also, over the years, the hydraulic conditions have changed due to natural erosion of the riverbed.

EXAMPLE 4 - Design deficiency possibly due to mistaken determination of hydrological conditions



$P_{11} = 19.4$



$P_{11} = 23.4$

BULB_X8_CCC

Eff = 86.01 %

Sigma_bl = 1.826

n11= 234.3

Q11= 2.62



BULB_X8_CCC

Eff = 87.04 %

Sigma_bl = 1.689

n11= 234.2

Q11= 2.6



BULB_X8_CCC

Eff = 85.89 %

Sigma_bl = 1.637

n11= 233.1

Q11= 2.46



BULB_X8_CCC

Eff = 85.52 %

Sigma_bl = 1.647

n11= 233.2

Q11= 2.44



BULB_X8_CCC

Eff = 85.11 %

Sigma_bl = 1.644

n11= 233.2

Q11= 2.43



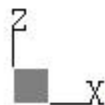
BULB_X8_CCC

Eff = 85.95 %

Sigma_bl = 1.609

n11= 233

Q11= 2.42



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BULB_X8_CCC

Eff = 86.41 %

Sigma_bl = 1.555

n11= 232.8

Q11= 2.41



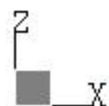
BULB_X8_CCC

Eff = 86.72 %

Sigma_bl = 1.552

n11= 232.5

Q11= 2.4



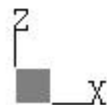
BULB_X8_CCC

Eff = 86.85 %

Sigma_bl = 1.47

n11= 232

Q11= 2.37



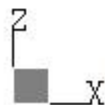
BULB_X8_CCC

Eff = 86.92 %

Sigma_bl = 1.463

n11= 232

Q11= 2.37



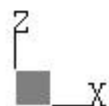
BULB_X8_CCC

Eff = 87.04 %

Sigma_bl = 1.45

n11= 231.6

Q11= 2.35



BULB_X8_CCC

Eff = 87.22 %

Sigma_bl = 1.438

n11= 231.8

Q11= 2.35



BULB_X8_CCC

Eff = 87.26 %

Sigma_bl = 1.433

n11= 231.8

Q11= 2.35



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BULB_X8_CCC

Eff = 87.33 %

Sigma_bl = 1.427

n11= 231.8

Q11= 2.36



BULB_X8_CCC

Eff = 87.86 %

Sigma_bl = 1.352

n11= 231.7

Q11= 2.34



BULB_X8_CCC

Eff = 88.1 %

Sigma_bl = 1.314

n11= 231.7

Q11= 2.33



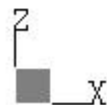
BULB_X8_CCC

Eff = 88.25 %

Sigma_bl = 1.29

n11= 231.6

Q11= 2.32



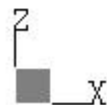
BULB_X8_CCC

Eff = 88.3 %

Sigma_bl = 1.233

n11= 231.5

Q11= 2.3



BULB_X8_CCC

Eff = 88.35 %

Sigma_bl = 1.234

n11= 231.5

Q11= 2.3



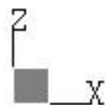
BULB_X8_CCC

Eff = 88.7 %

Sigma_bl = 1.197

n11= 231.7

Q11= 2.29



BULB_X8_CCC

Eff = 88.76 %

Sigma_bl = 1.071

n11= 231.6

Q11= 2.26



BULB_X8_CCC

Eff = 89.32 %

Sigma_bl = 1.031

n11= 231.4

Q11= 2.29



BULB_X8_CCC

Eff = 89.74 %

Sigma_bl = 1.036

n11= 231.4

Q11= 2.3



BULB_X8_CCC

Eff = 89.98 %

Sigma_bl = 1.032

n11= 231.6

Q11= 2.38



BULB_X8_CCC

Eff = 90.25 %

Sigma_bl = 1.015

n11= 231.6

Q11= 2.38



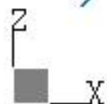
BULB_X8_CCC

Eff = 90.24 %

Sigma_bl = 1.058

n11= 231.6

Q11= 2.41



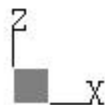
BULB_X8_CCC

Eff = 90.42 %

Sigma_bl = 1.014

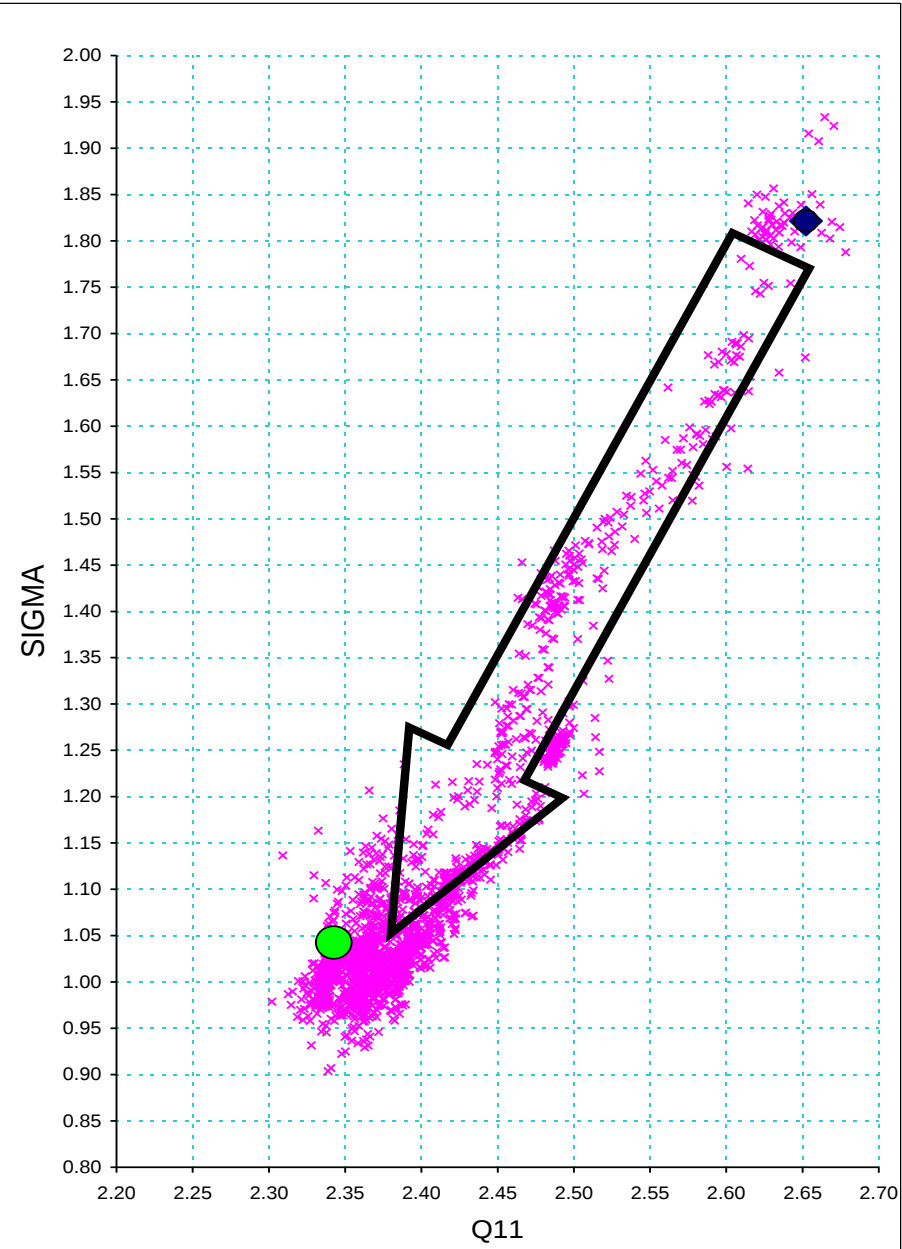
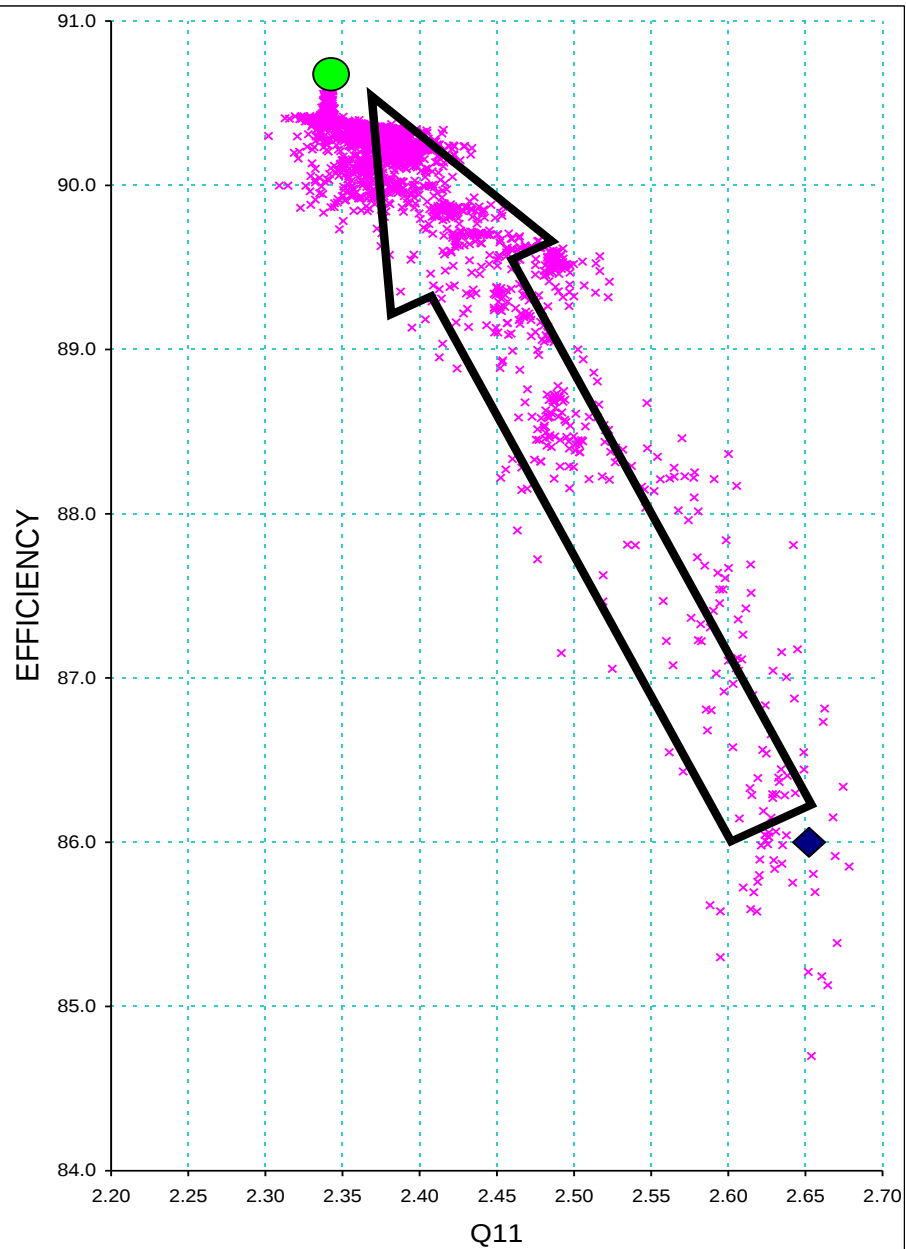
n11= 231.4

Q11= 2.34

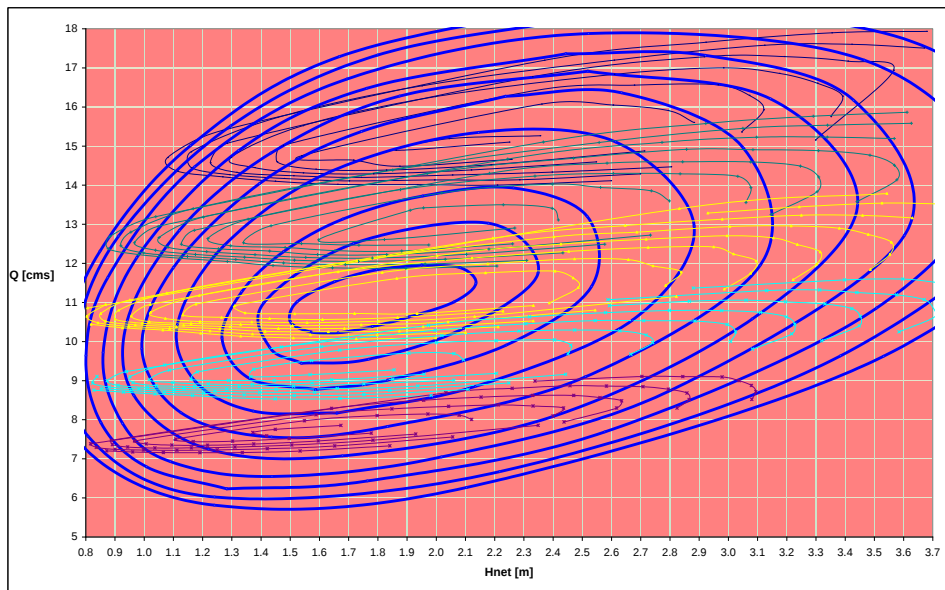
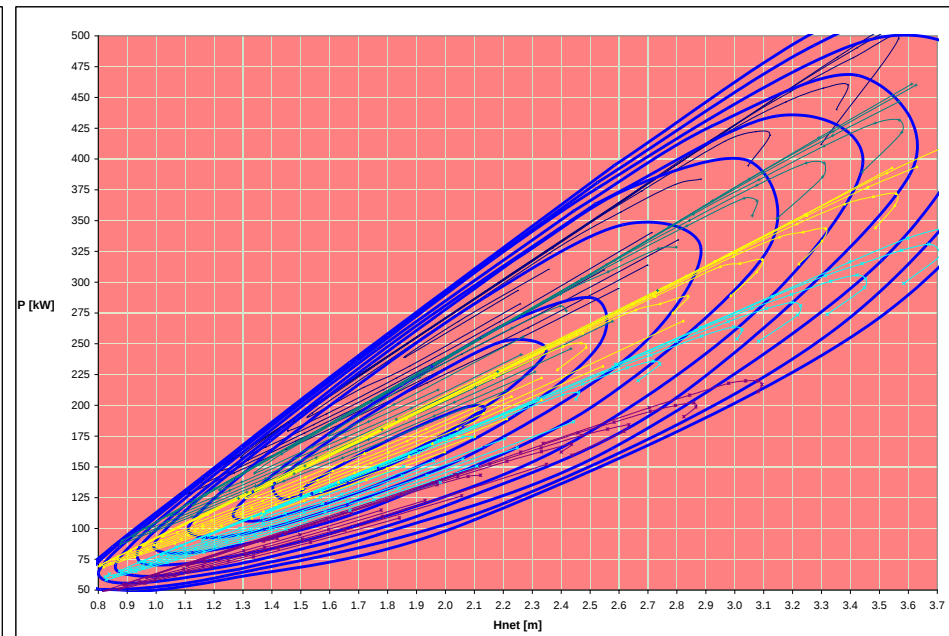
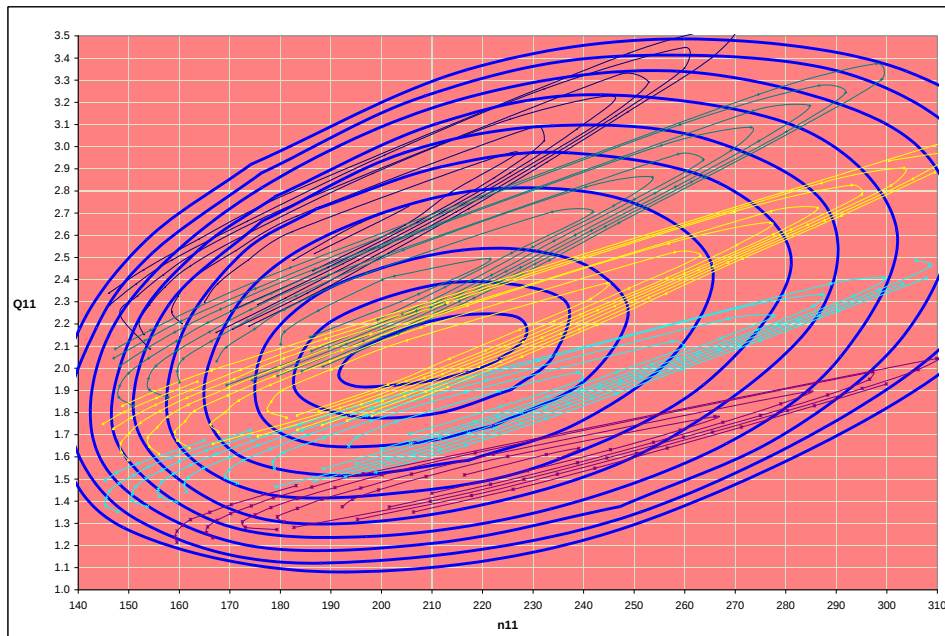


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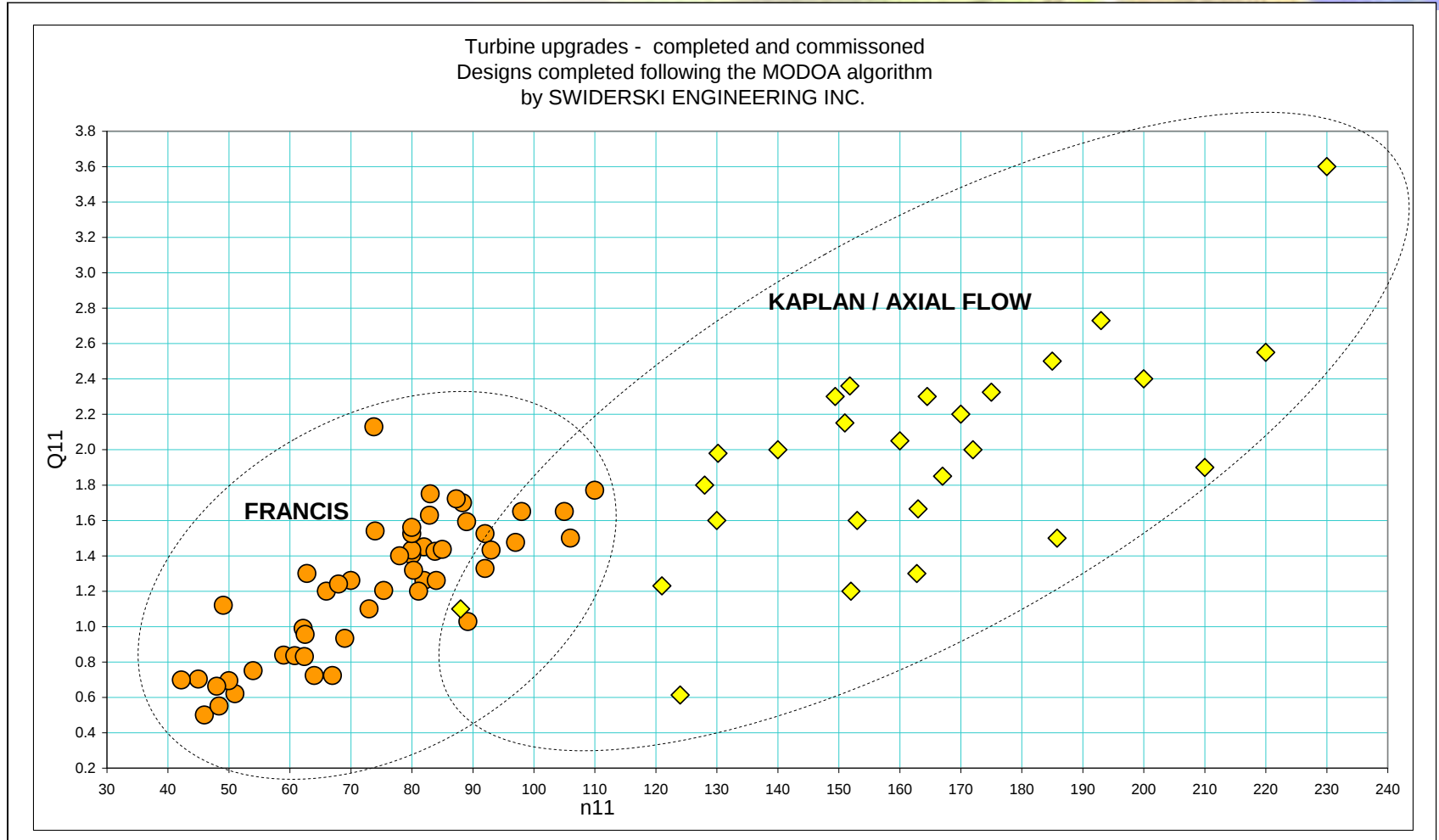
Optimization process - history



Optimized turbine – hill chart

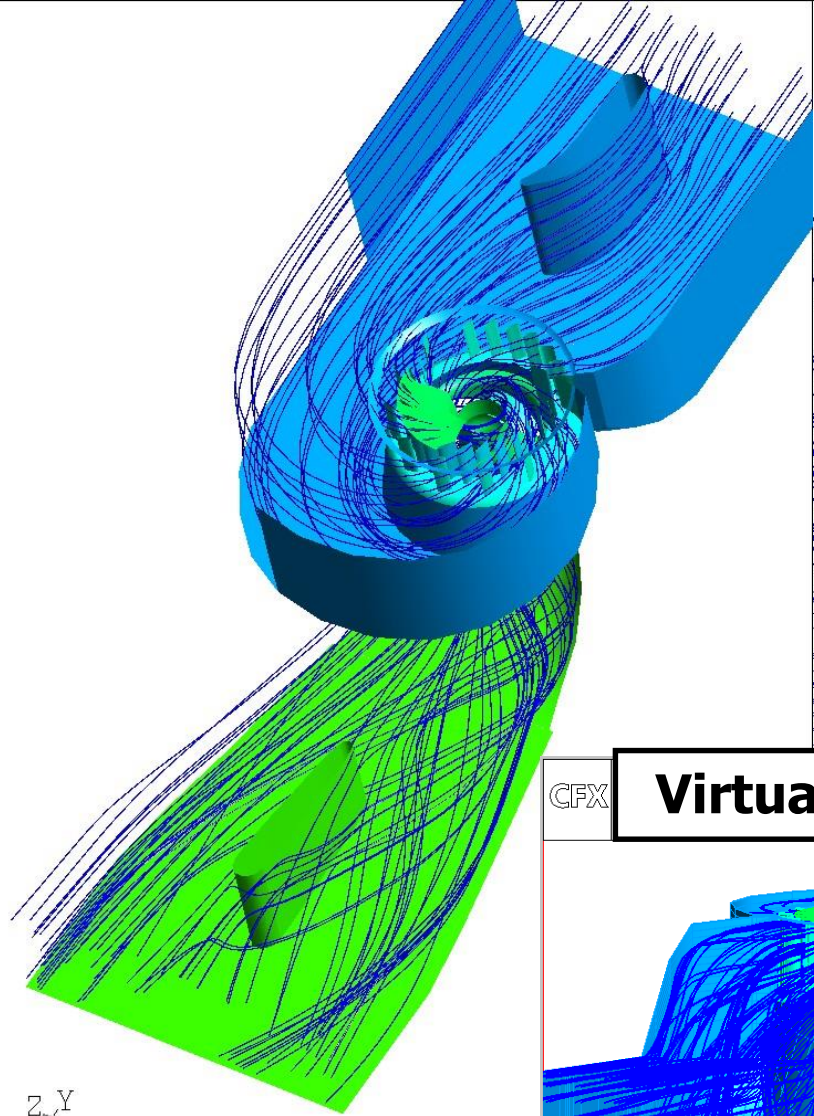


Modernizations completed



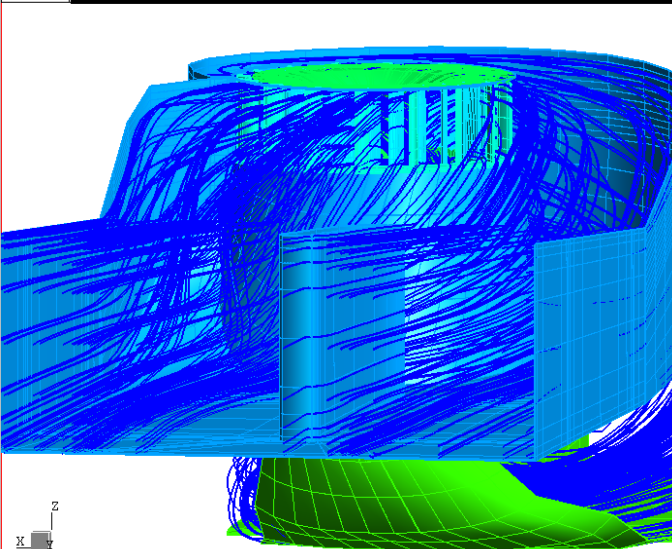
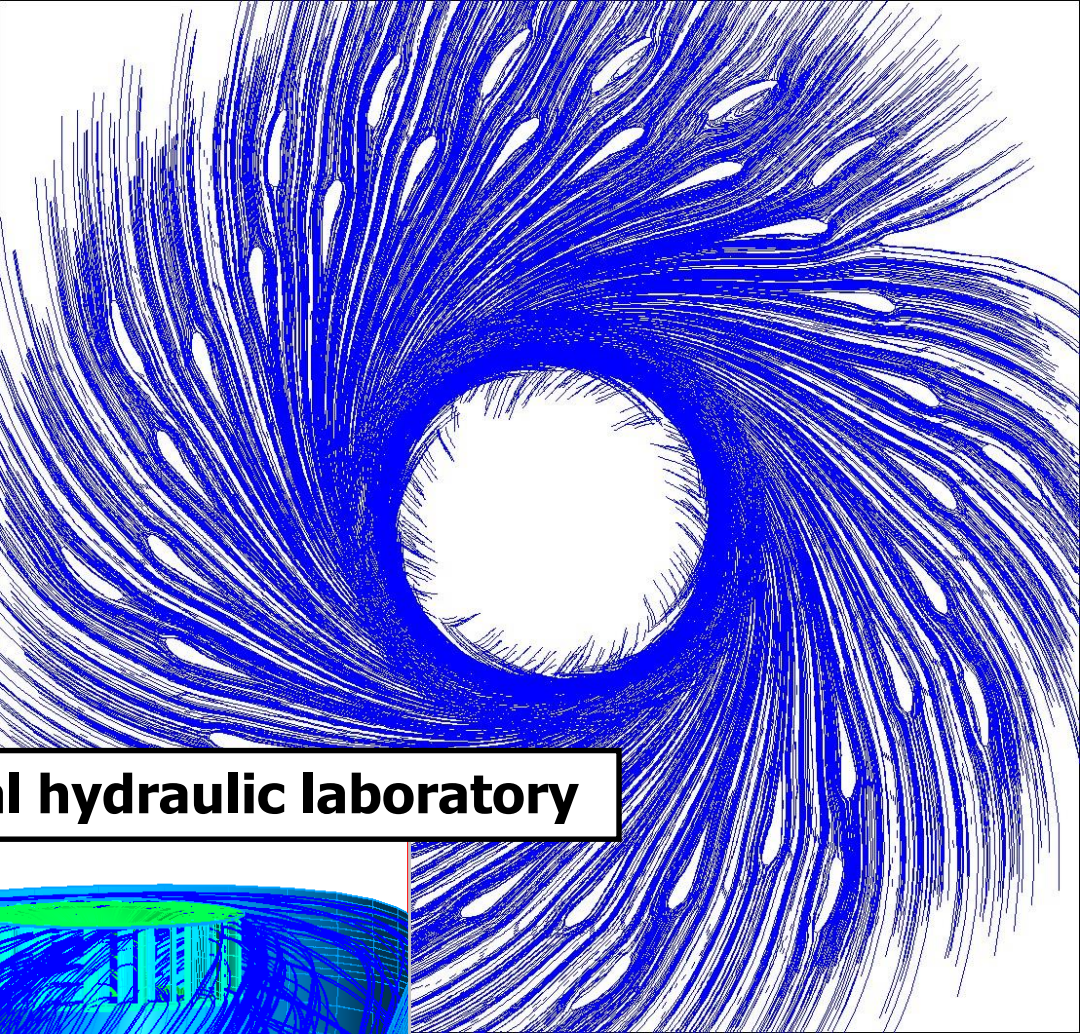
56 designs of Francis turbines or runners were completed, over 117 runners built.

27 designs of Kaplan and/or Axial Flow turbines were completed, 39 runners built.



CFX

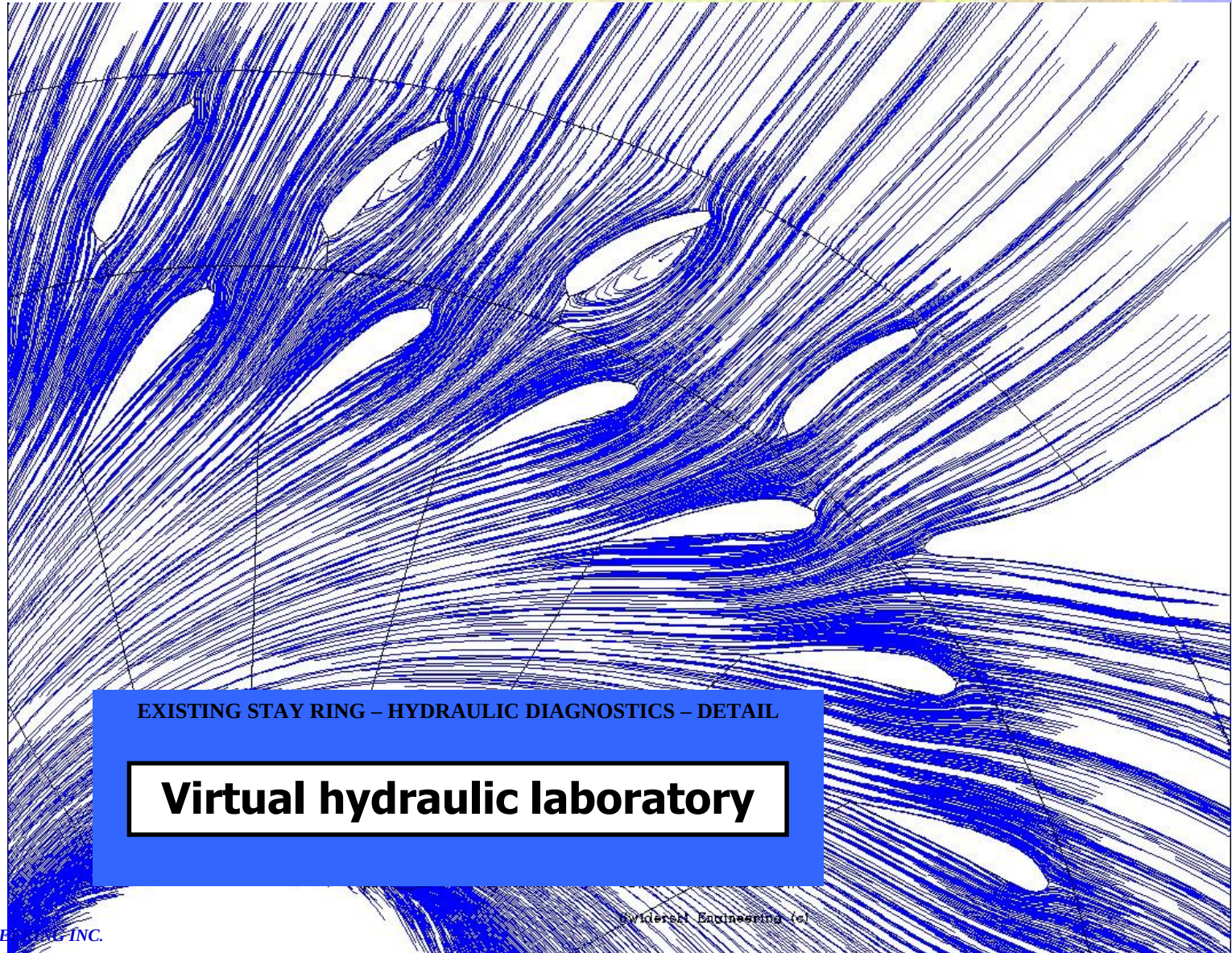
Virtual hydraulic laboratory



Z
Y
X

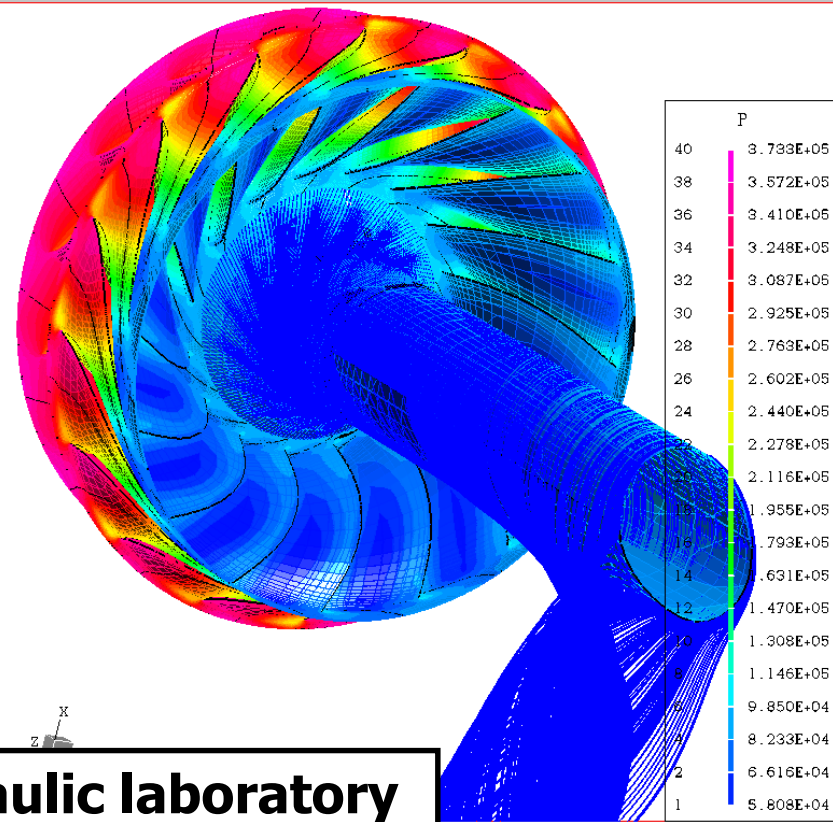
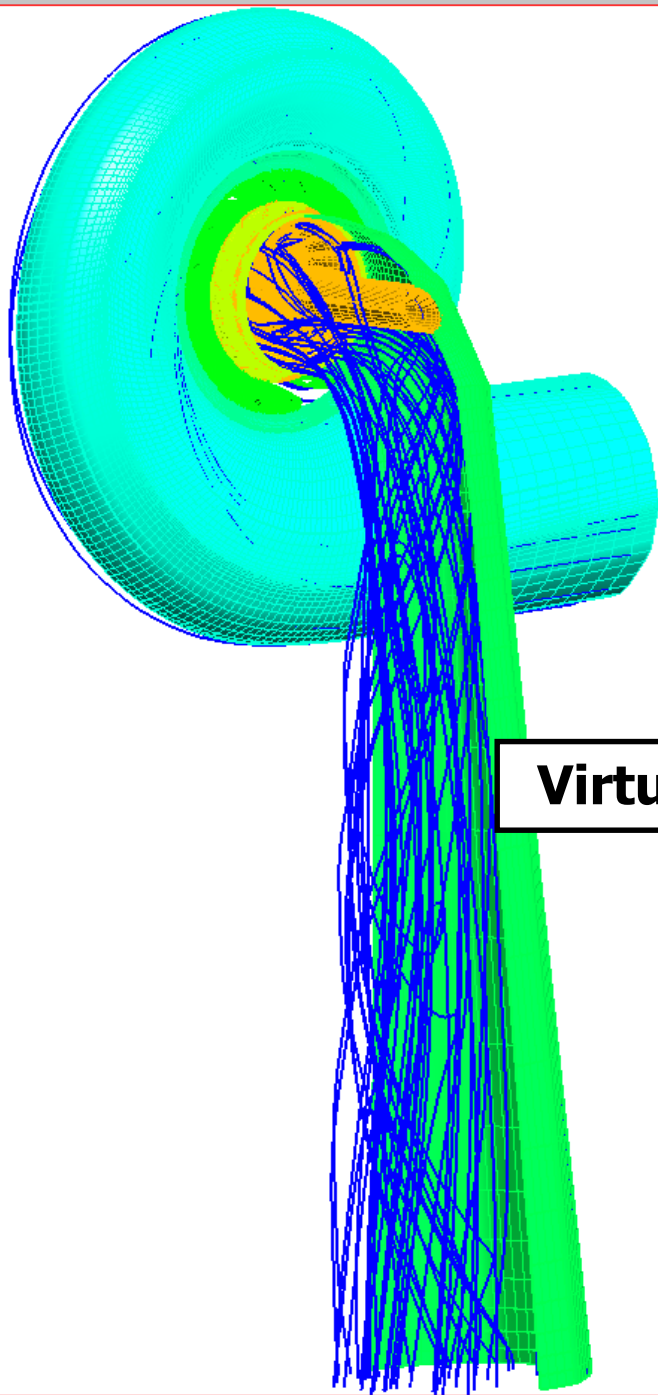
Z
X

Hudraulic diagnostics – sample 1

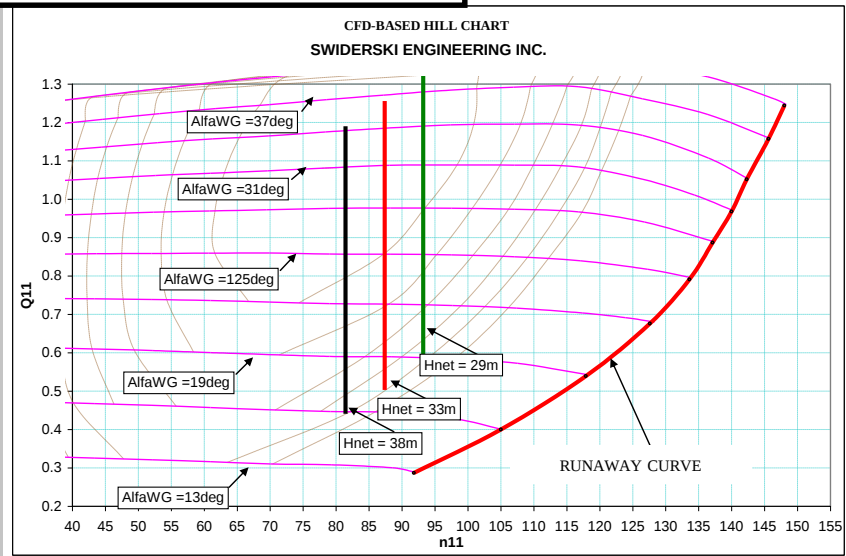


EXISTING STAY RING – HYDRAULIC DIAGNOSTICS – DETAIL

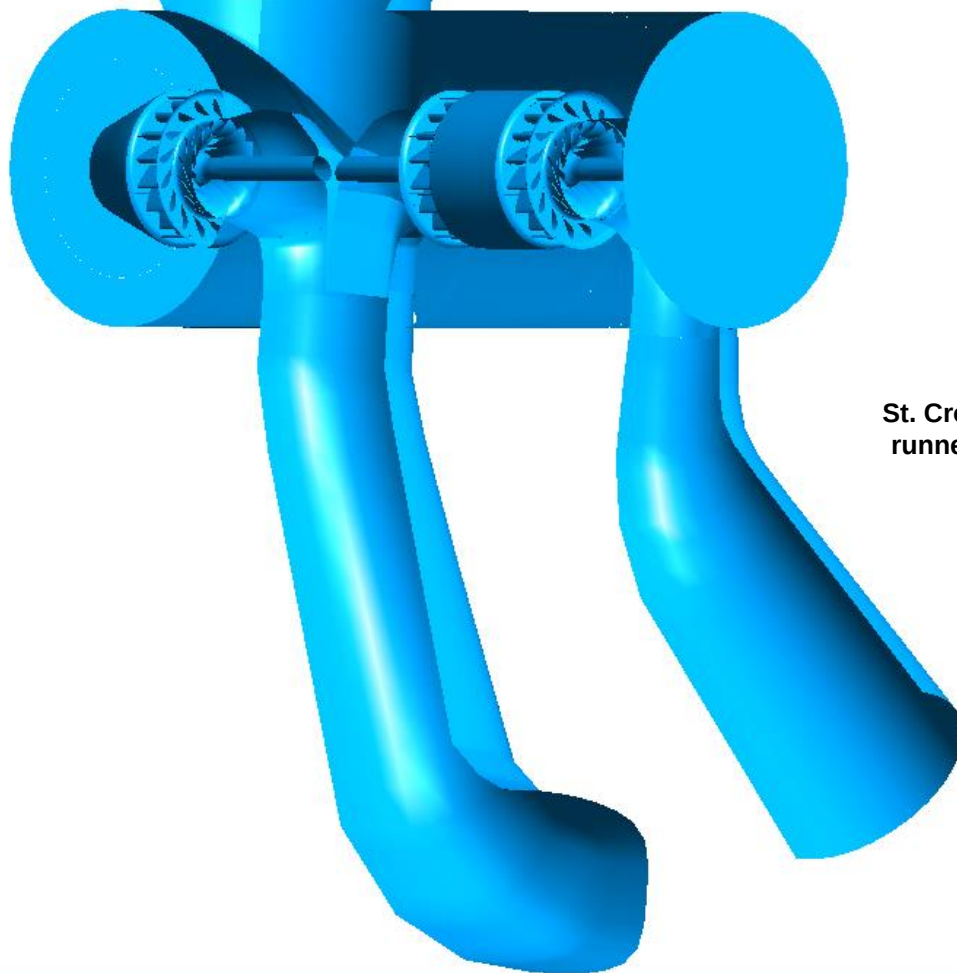
Virtual hydraulic laboratory



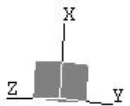
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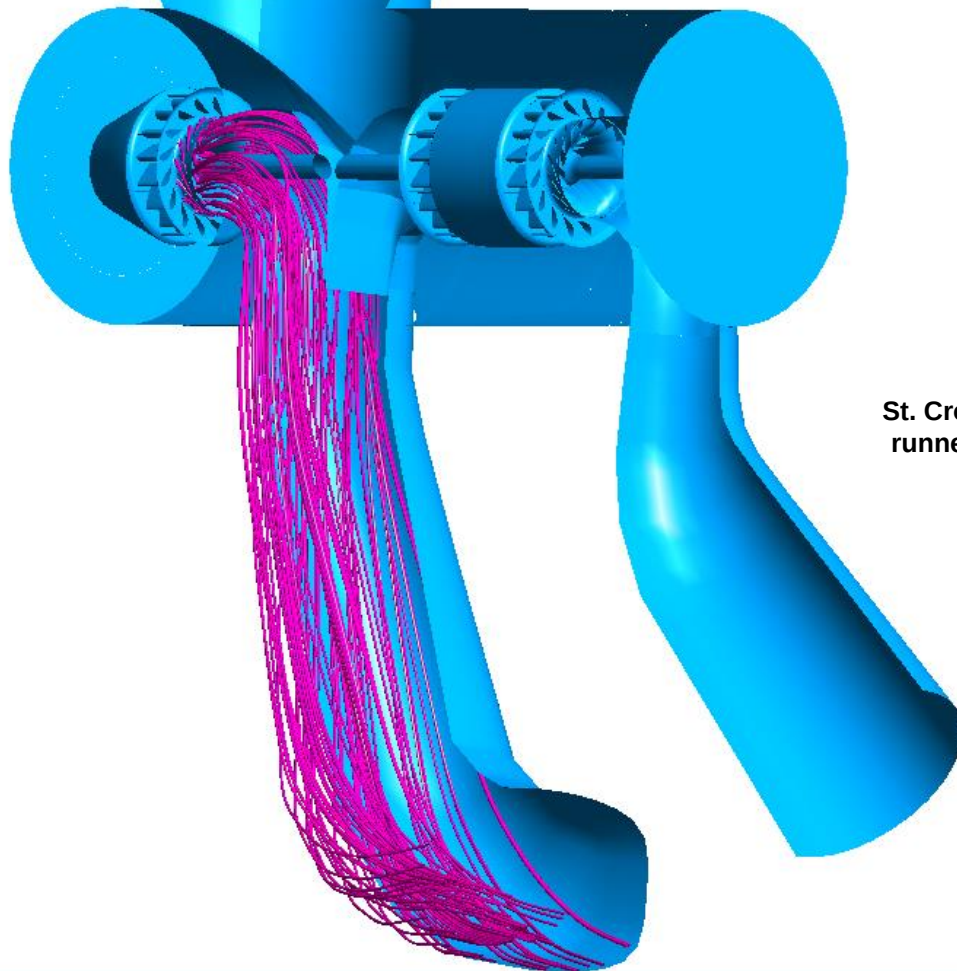
Virtual hydraulic laboratory



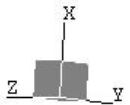
St. Croix Project –
runners upgrade



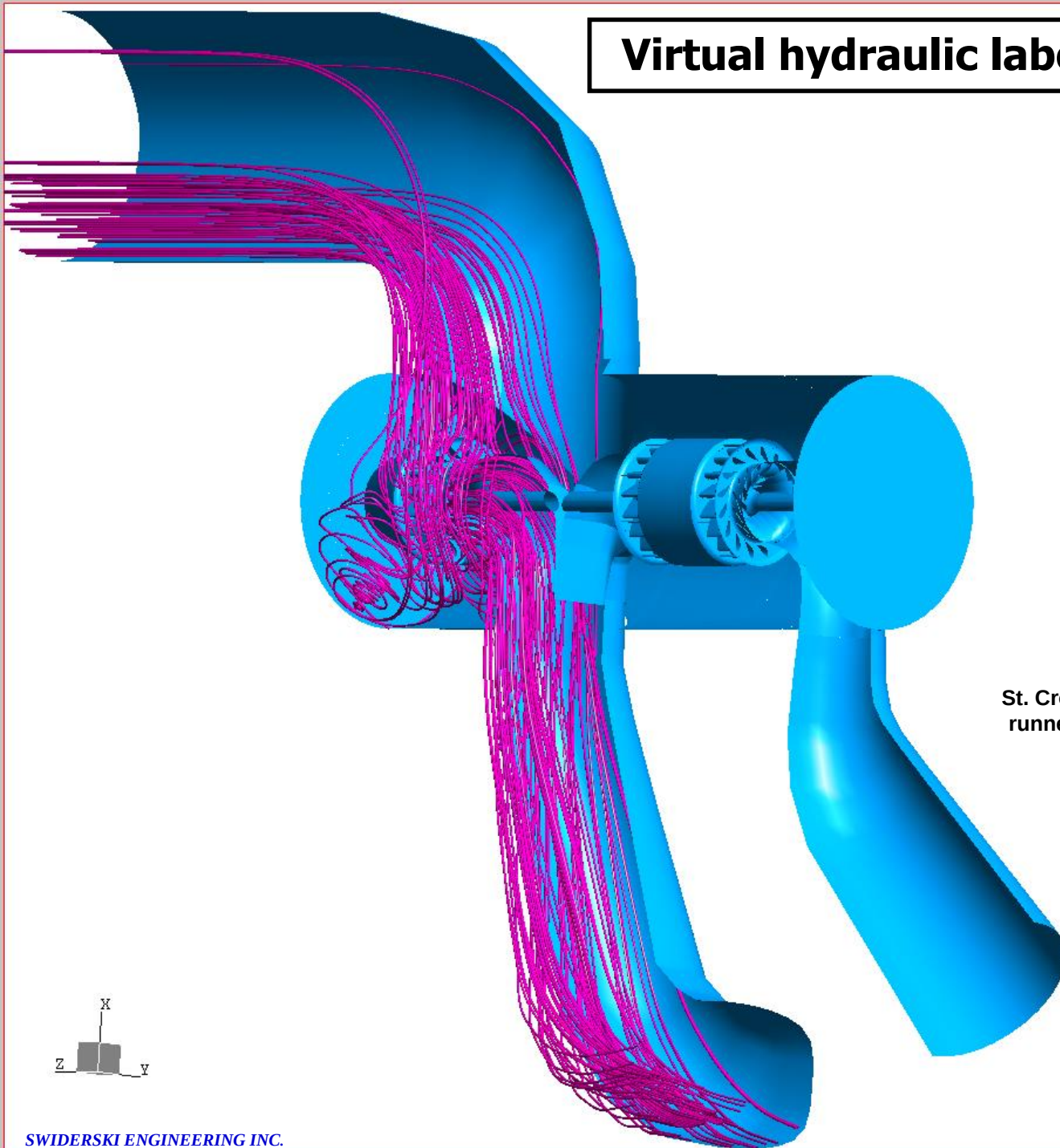
Virtual hydraulic laboratory



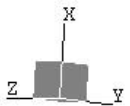
St. Croix Project –
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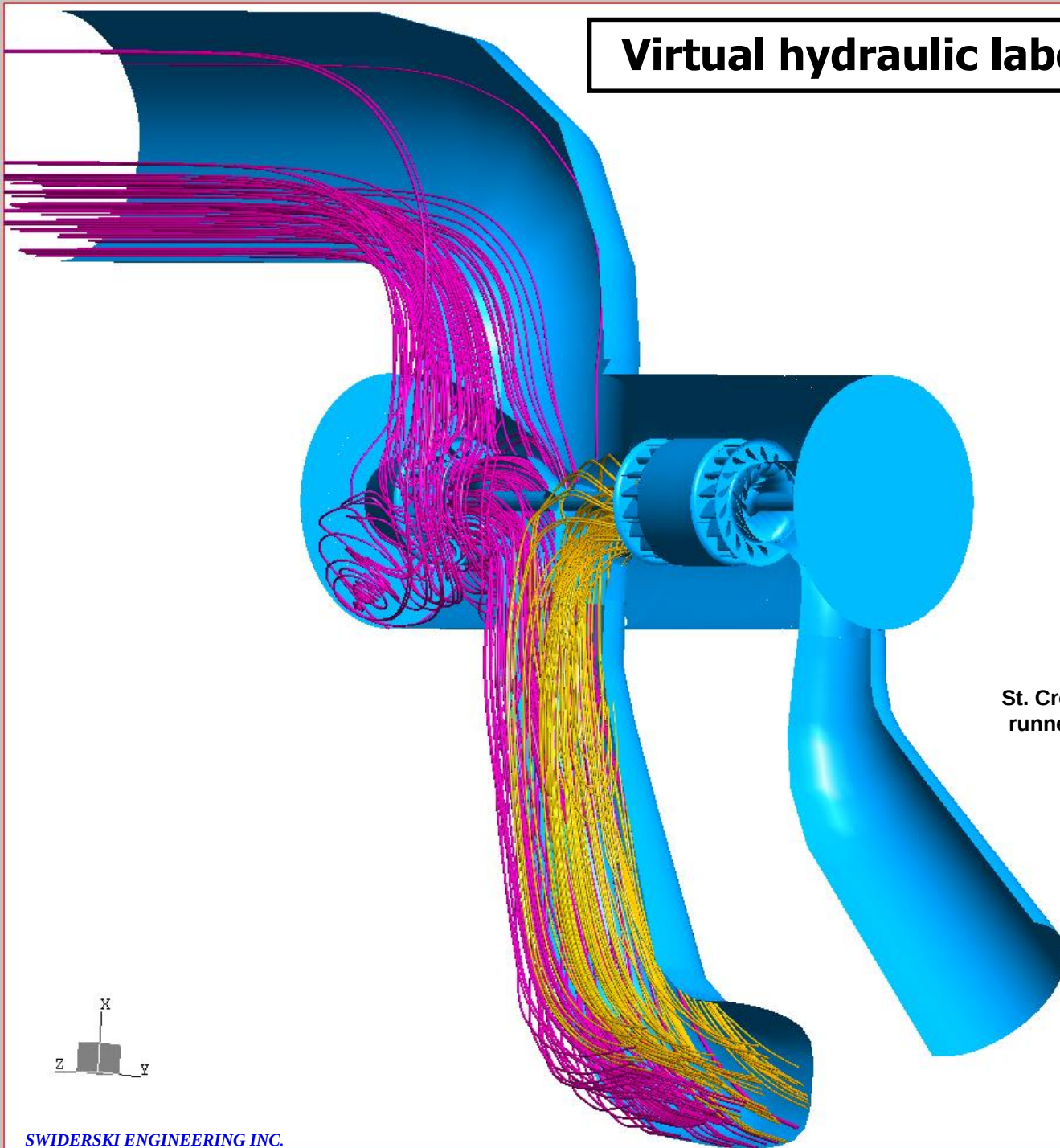
Virtual hydraulic laboratory



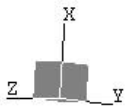
St. Croix Project –
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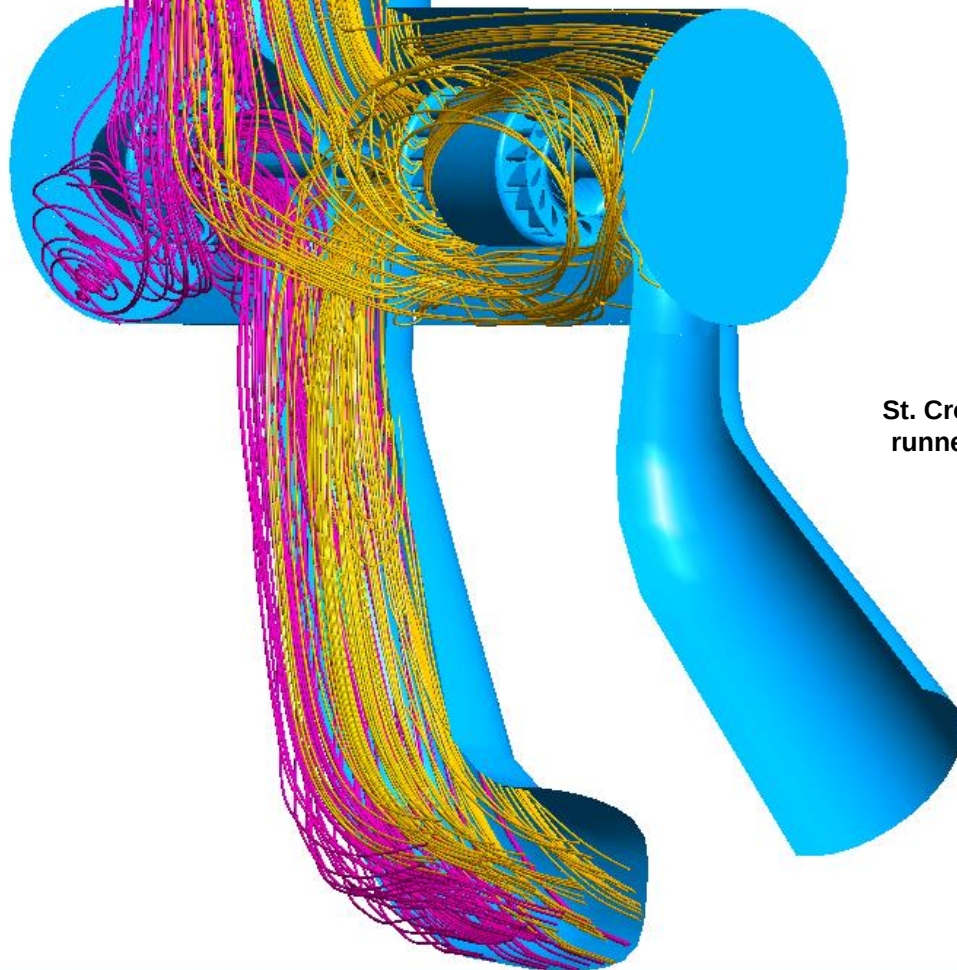
Virtual hydraulic laboratory



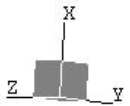
St. Croix Project –
runners upgrade



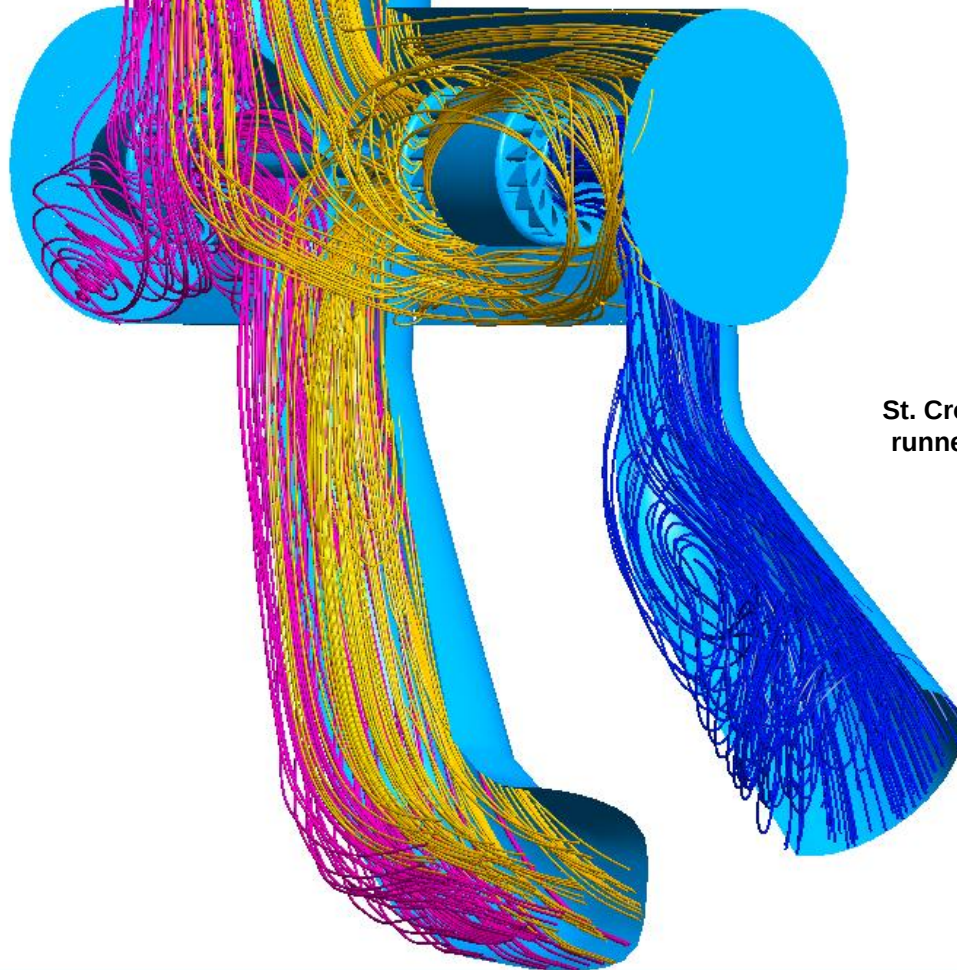
Virtual hydraulic laboratory



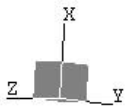
St. Croix Project –
runners upgrade



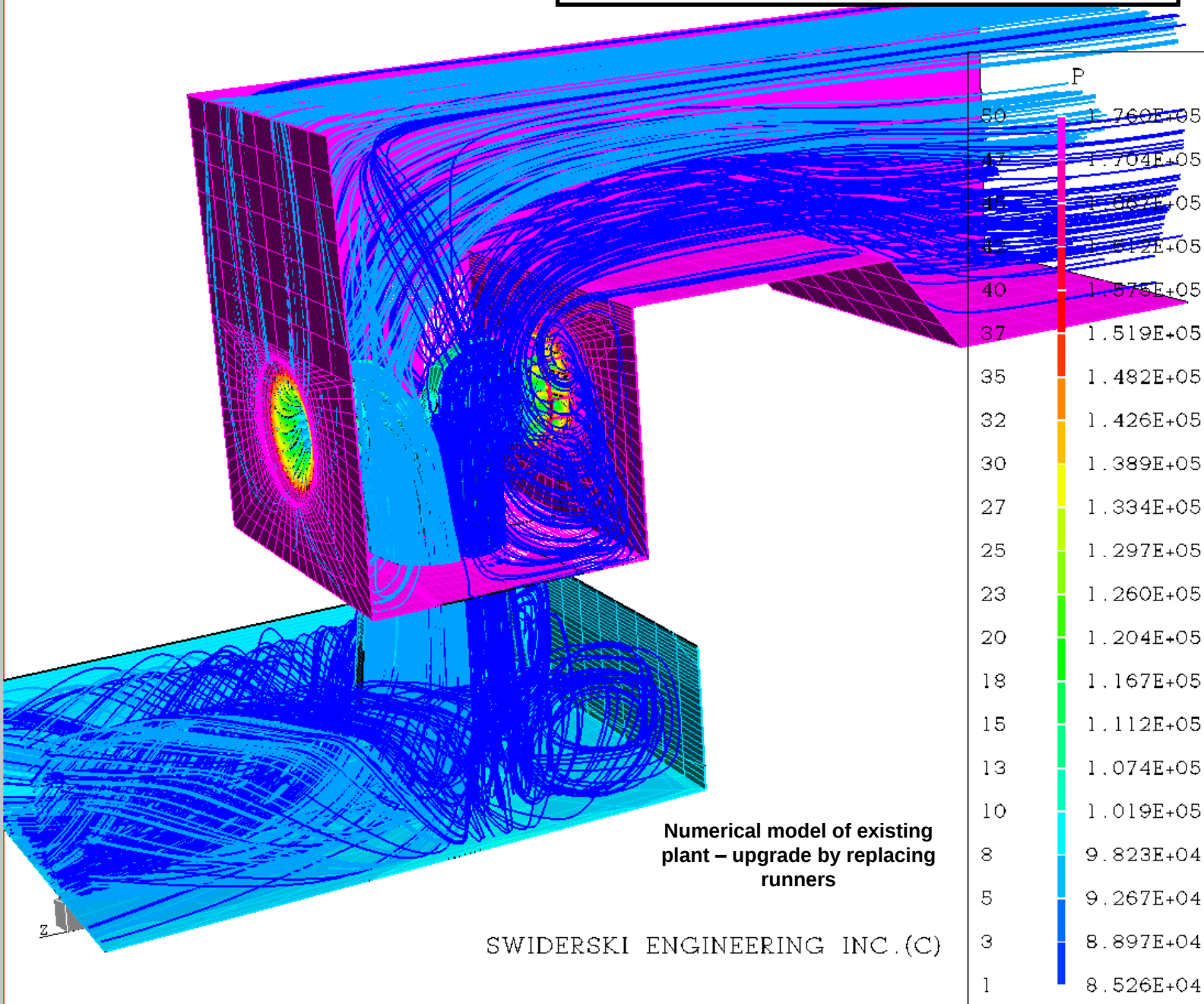
Virtual hydraulic laboratory

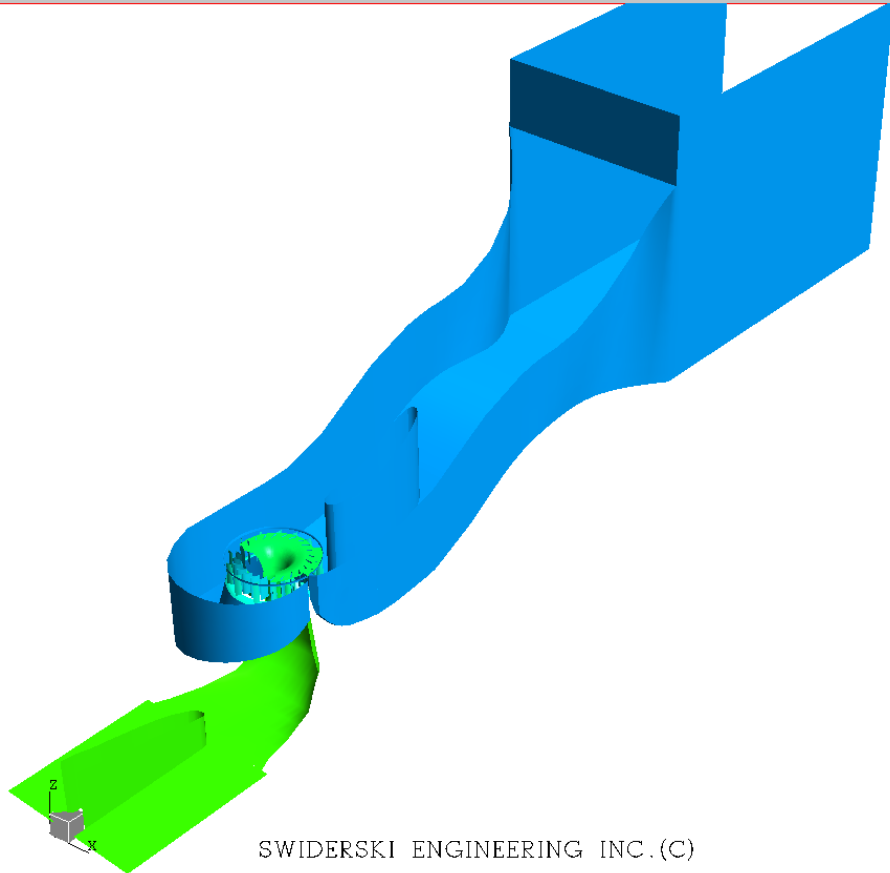


St. Croix Project –
runners upgrade

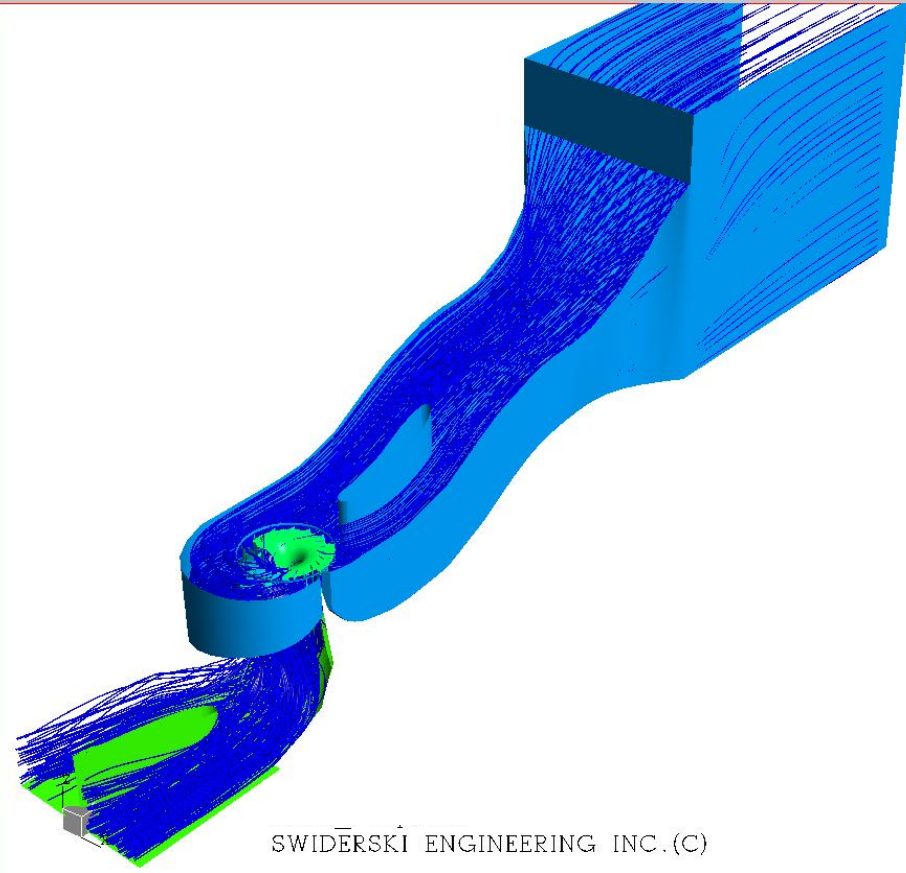


Virtual hydraulic laboratory

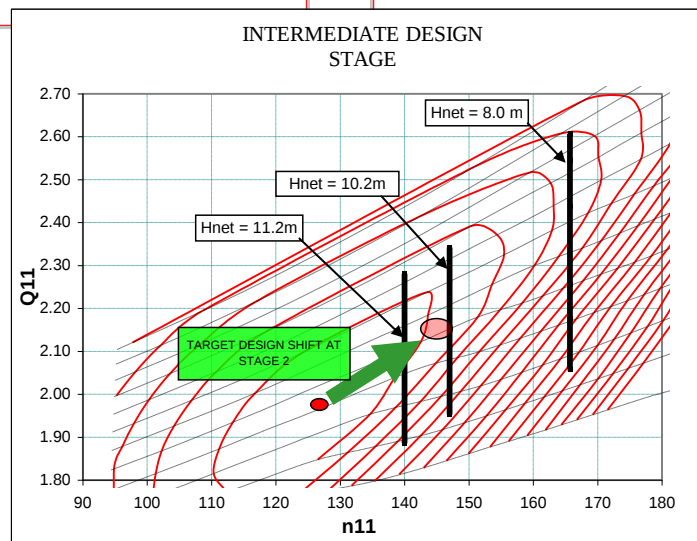




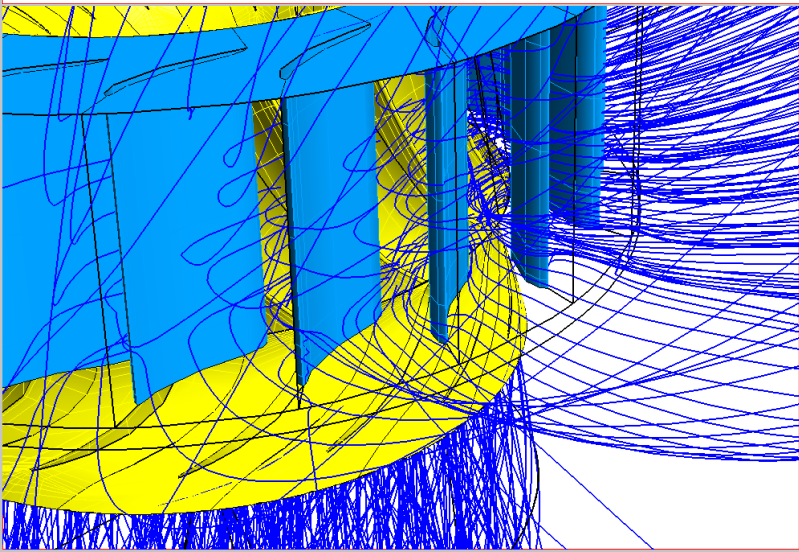
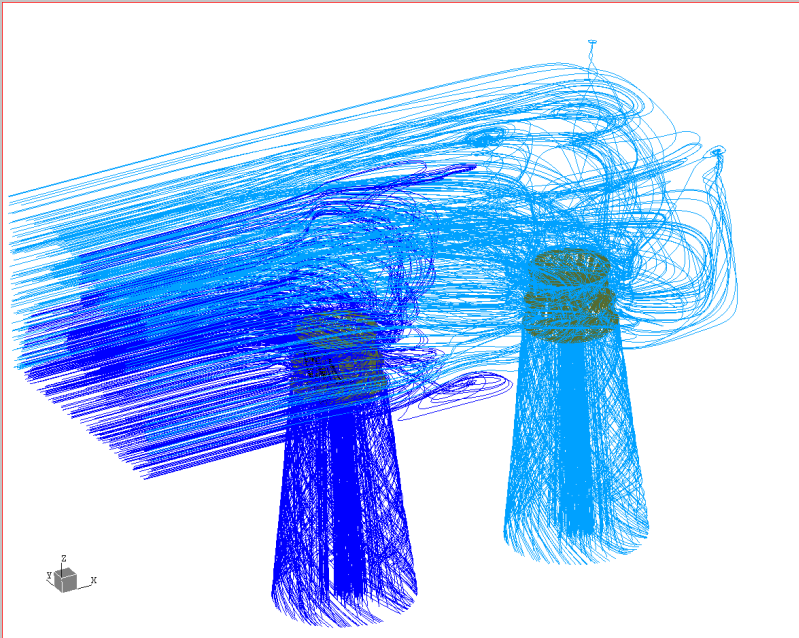
SWIDERSKI ENGINEERING INC.(C)



SWIDERSKI ENGINEERING INC.(C)

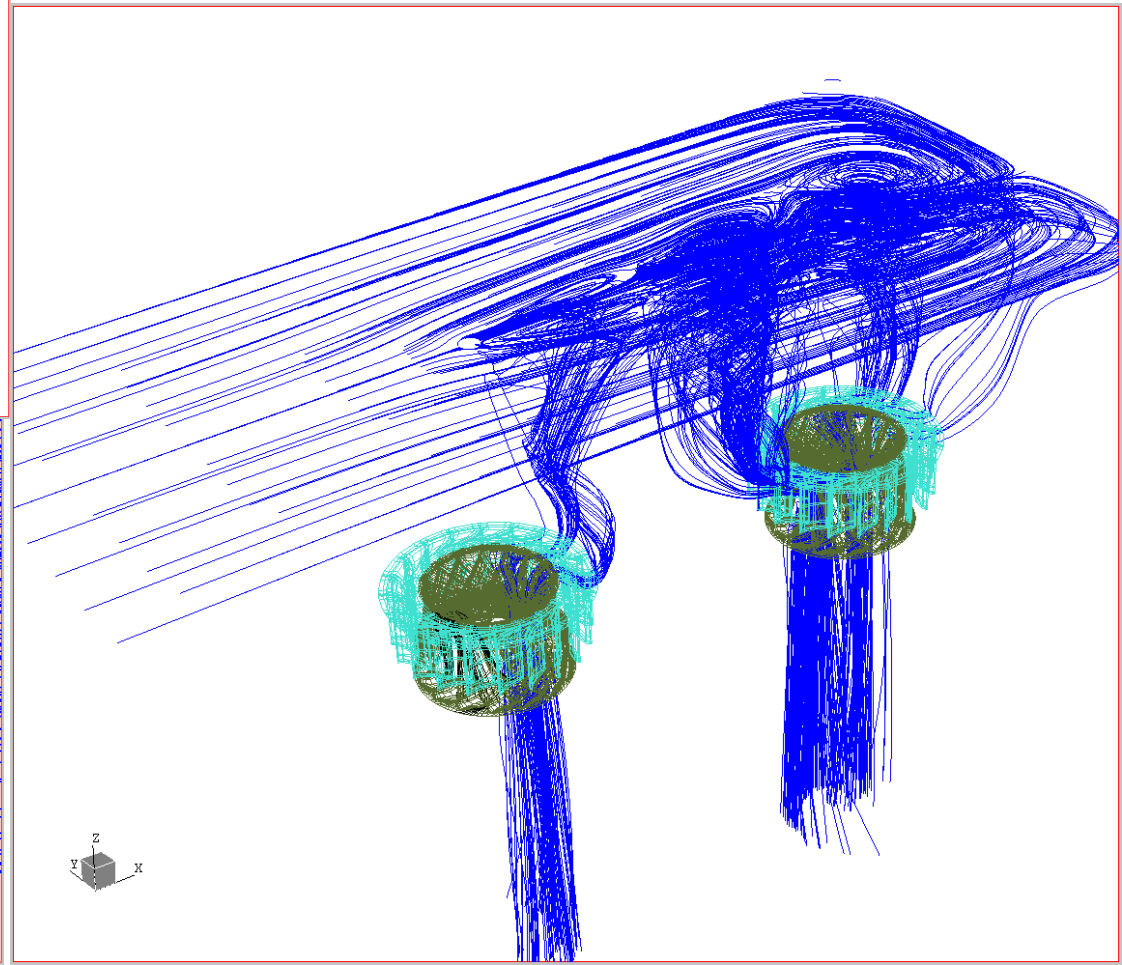


Hydraulic diagnostics – sample 2

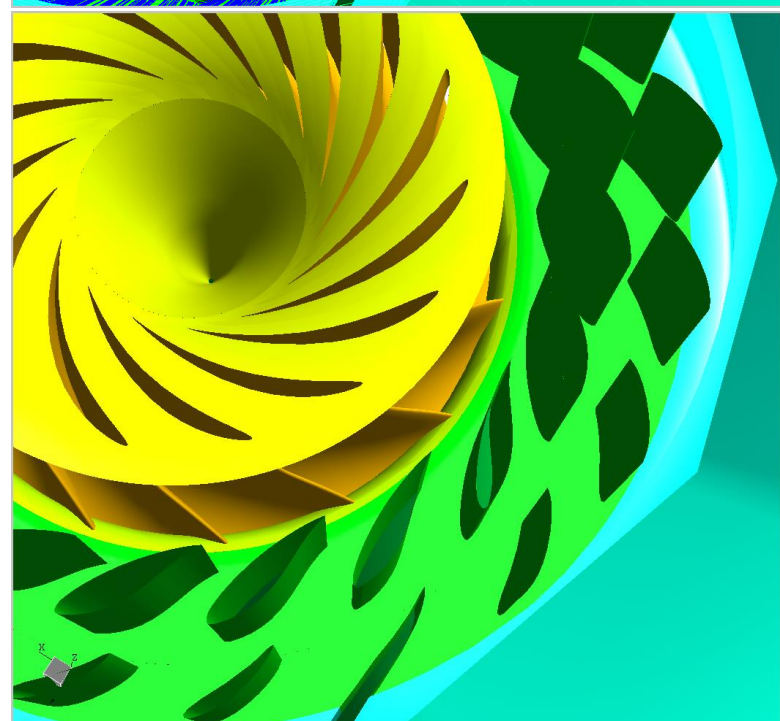
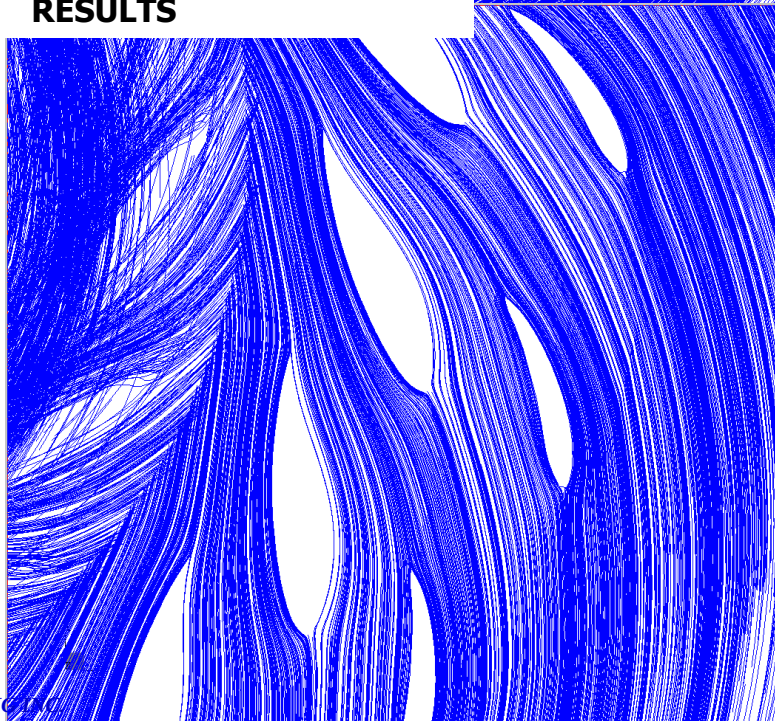
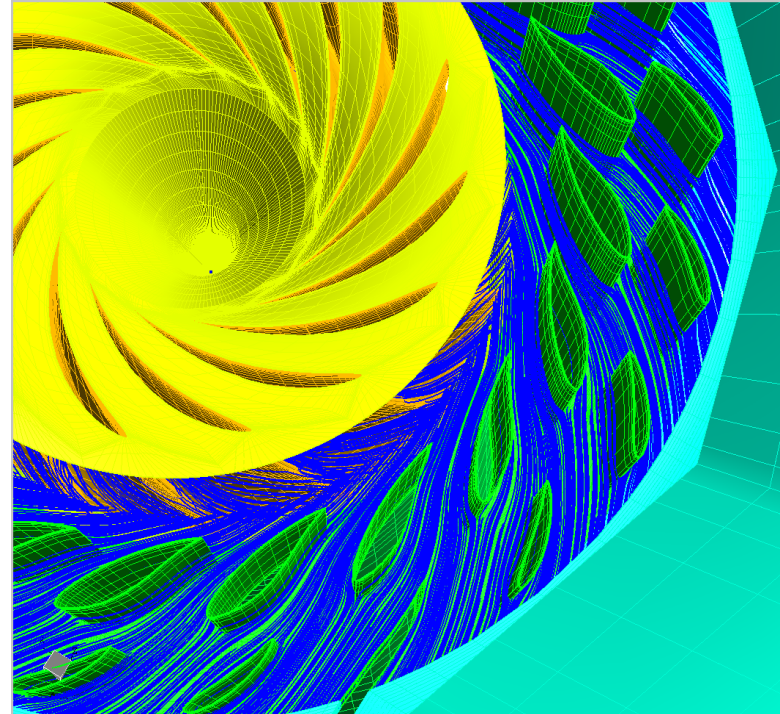
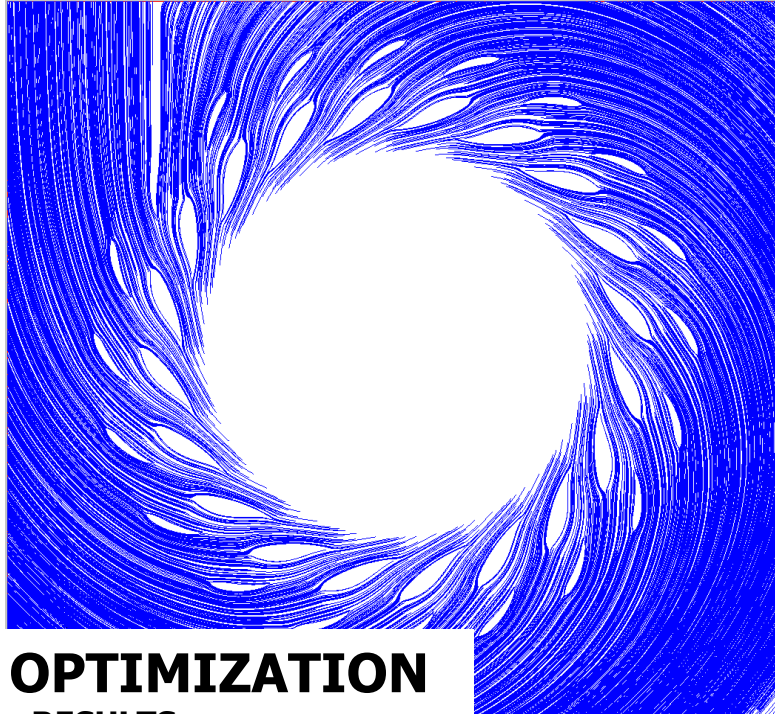


GLENN FERRIS PROJECT

UNITS 1 - 6

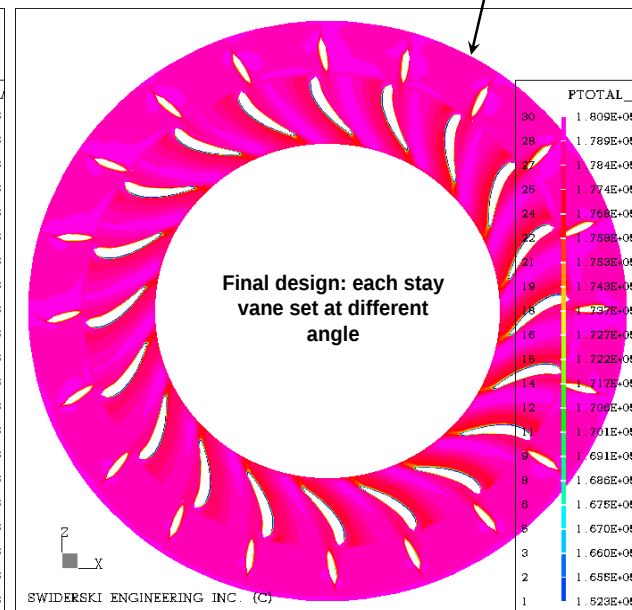
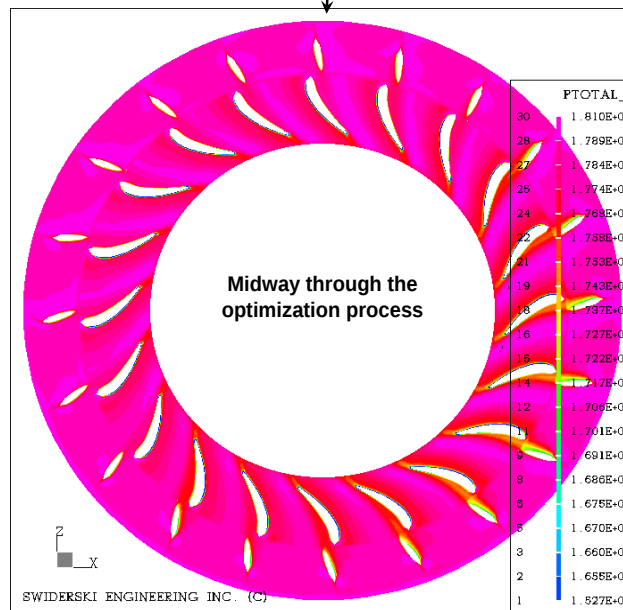
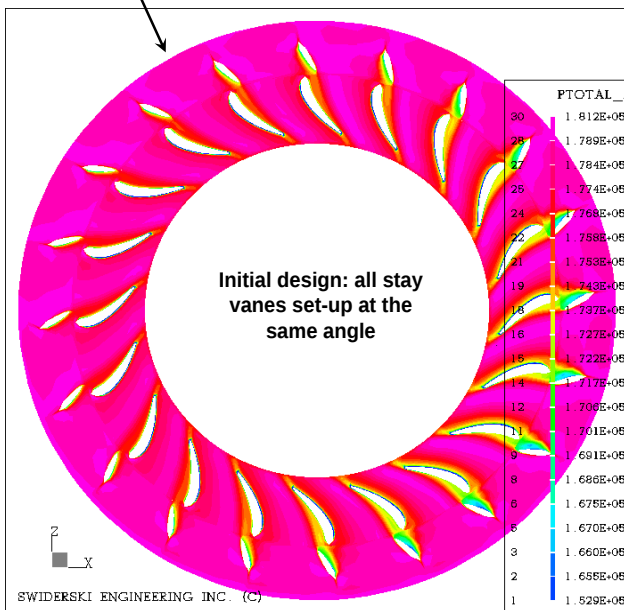
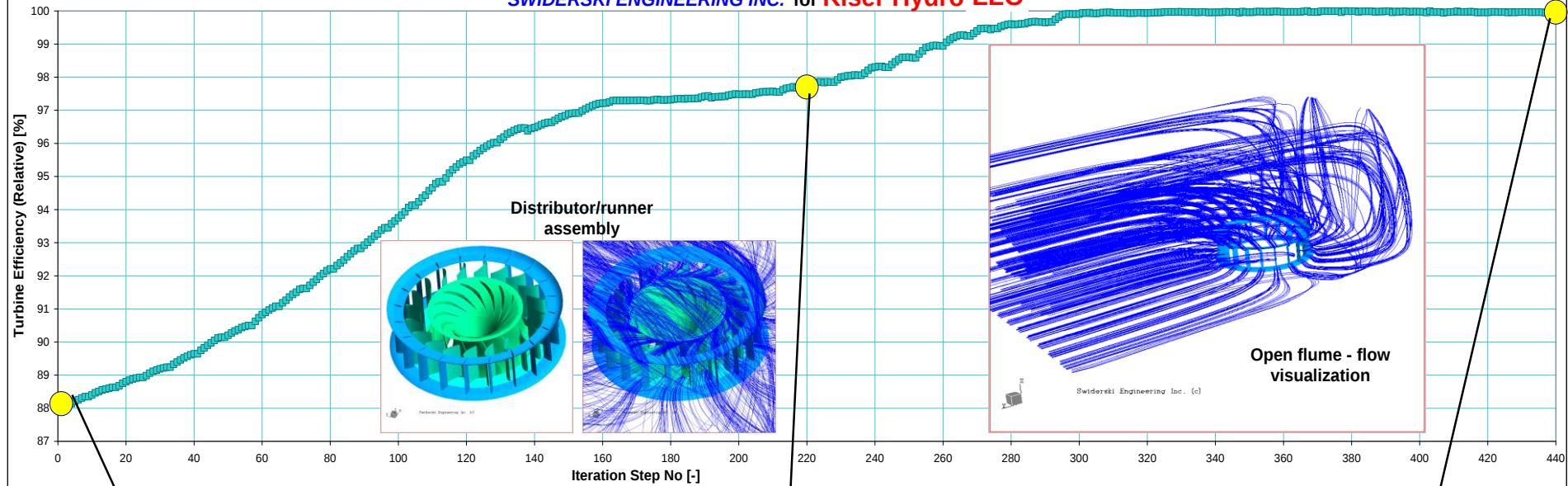


DESIGN OPTIMIZATION RESULTS



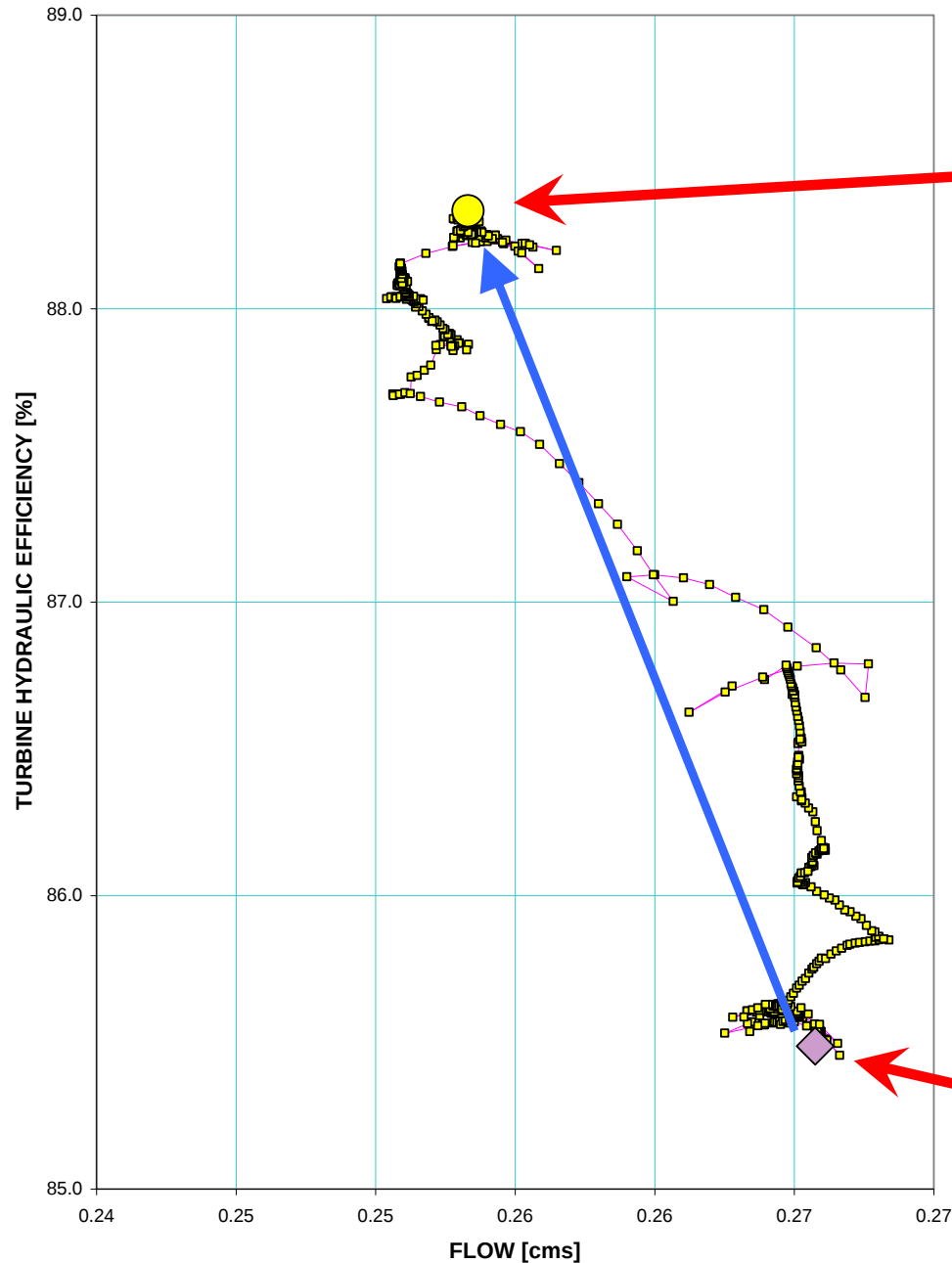
Stay Vanes set-up optimization open flume Francis turbine

SWIDERSKI ENGINEERING INC. for Kiser Hydro LLC



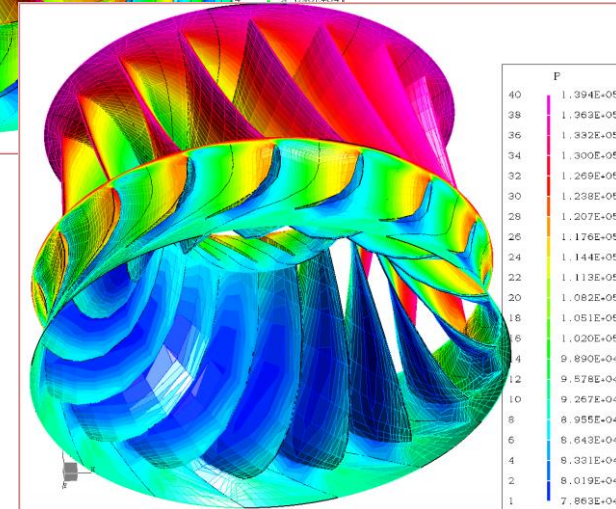
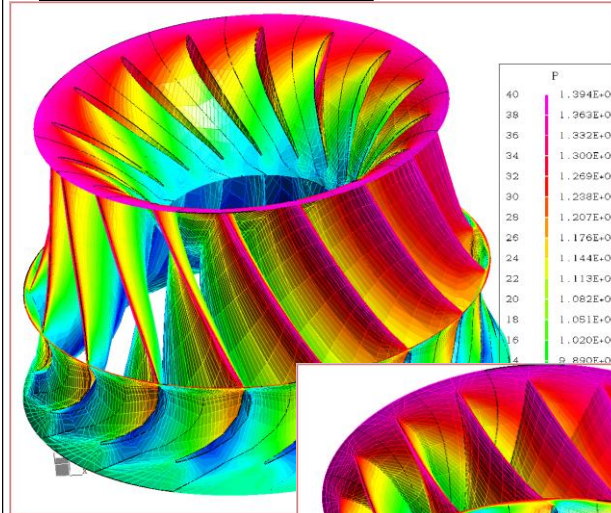
SOLUTION-DEPENDENT STAGE

SWIDERSKI ENGINEERING INC.



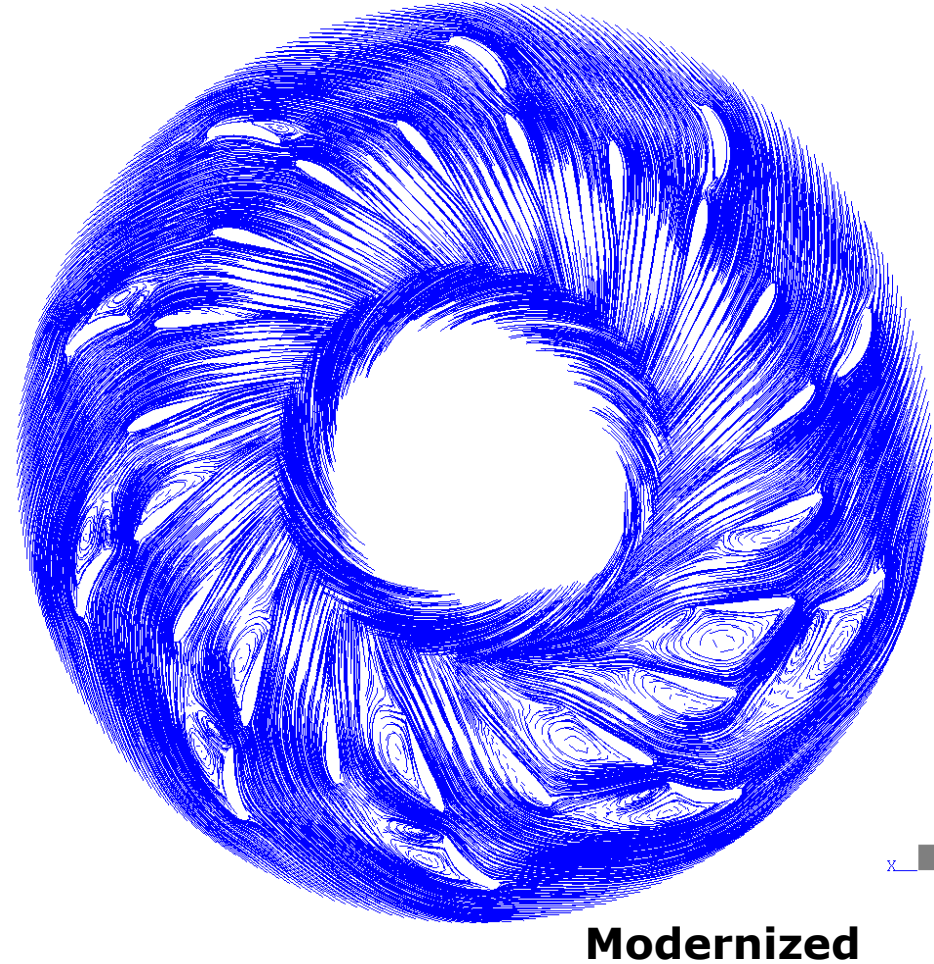
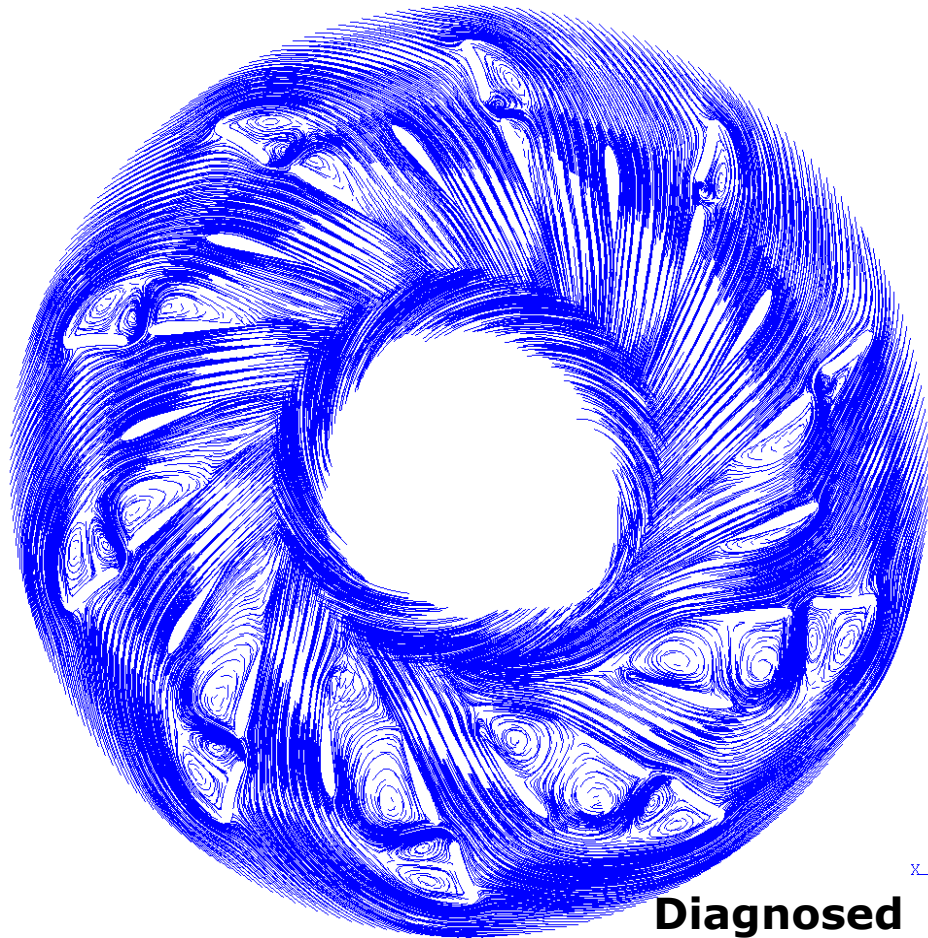
DESIGN OPTIMIZATION HISTORY OF THE PROCESS

DESIGN TARGET

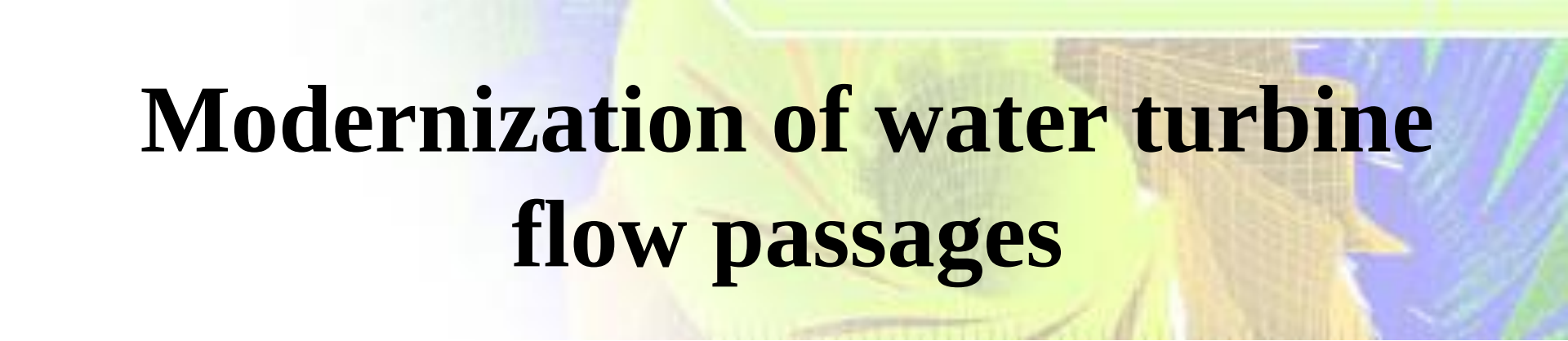


START - INITIAL GUESS

Hydraulic diagnostics – sample 3



Modification of the stay vanes resulted in approx. 8% increase in energy production



Modernization of water turbine flow passages

by
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THANK YOU